# THE SECOND CALTECH-JODRELL BANK VLBI SURVEY. II. OBSERVATIONS OF 102 OF 193 SOURCES

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# ABSTRACT

This is the second of two papers presenting the Second Caltech–Jodrell Bank VLBI survey (CJ2). The CJ2 sample consists of 193 flat- and gigahertz-peaked–spectrum sources selected at 4850 MHz. In this paper we present images of the remaining 102 sources with a resolution of  $\sim 1$  mas, obtained using VLBI snapshot observations at 4992 MHz with a global array. We also present integrated radio spectra for the entire CJ2 sample.

Subject headings: quasars: general — radio continuum: galaxies — surveys

## 1. INTRODUCTION

The second Caltech–Jodrell Bank VLBI survey (CJ2) is a Mark II snapshot VLBI survey of 193 flat- and gigahertzpeaked–spectrum radio sources, observed at a frequency of 4992 MHz. The main aims of CJ2 are to extend the morphological classification started by the Pearson & Readhead survey (Pearson & Readhead 1988, hereafter PR), and first Caltech– Jodrell Bank VLBI survey (Polatidis et al. 1995; Thakkar et al. 1995; Xu et al. 1995; hereafter CJ1) and to address three cosmological goals. These goals are (1) to place significant limits on the mass in  $10^{6}$ – $10^{9} M_{\odot}$  condensed objects by searching for gravitational lenses with a separation of 1–200 mas, (2) to look for evidence of cosmological evolution in the proper motions of superluminal sources and place limits on  $q_{0}$ , and (3) to explore the possibility of using the angular diameter– redshift diagram for compact objects to constrain  $q_{0}$ .

In the first paper in this series (Taylor et al. 1994), we defined the CJ2 sample. We also reported on the first three observing sessions and presented VLBI images of 91 sources. We showed that the images, including those presented in this paper, are predominantly limited by thermal noise and not by dynamic range. Hence CJ2 is an excellent, uniform sample of VLBI images, ideal for the statistical tests which are the aims of the survey.

In this paper we present the second half of the results of the CJ2 survey. In § 2 we describe the fourth and final observing session, and in § 3 we present VLBI images of the remaining 102 sources. In § 4 we present integrated radio spectra, compiled from the literature, for all 193 sources in the CJ2 sample.

A redshift program of observations of CJ2 sources which have no measured redshift is well underway (Vermeulen & Taylor 1995);  $\sim$ 70% of CJ2 sources now have a measured redshift.

## 2. OBSERVATIONS

The observations presented in this paper were made from 1993 June 9 to June 16. Thirteen telescopes from the European VLBI Network (EVN), the US National Radio Astronomy Observatory's Very Large Baseline Array<sup>1</sup> (VLBA; Napier et al. 1994), and the VLA<sup>1</sup> participated successfully. Their characteristics are listed in Table 1. The observing frequency was 4992 MHz, and left-circular polarization was recorded using the Mark II system with 2 MHz bandwidth.

The VLBI snapshot technique was used, as in the previous sessions detailed in Paper I. Each source was observed for three to five scans of 20 minutes duration, the scans being approximately equally spaced over a wide range in hour angle. The sources observed in this session were mainly of low declination  $(\delta \sim 35^\circ - 50^\circ)$ , and since fewer telescopes observed successfully than in previous sessions, the *u*-*v* coverage was generally poorer than before. Figure 1 shows the typical *u*-*v* coverage for this session.

The data reduction procedure was identical to that given in Paper I, so only a brief outline will be given here. The data were correlated with the JPL/Caltech Block II correlator with clock offsets being monitored using strong calibrator sources. The data were then fringe-fitted using the AIPS task FRING, with a solution interval of  $\sim$ 7 minutes. Effelsberg was used as the reference telescope wherever possible; otherwise, the Hancock VLBA antenna was used. The amplitude calibration for each antenna, determined using measurements of antenna gain and system temperature, was adjusted by imaging strong calibrator sources and by examining the *u*-*v* crossing points. The relative amplitude calibration is accurate to  $\sim 2\%$  rms, and the absolute flux calibration is accurate to better than 10%. The data were phase self-calibrated to a point-source model with a 10 s solution interval and then coherently averaged to 1 minute. Finally, the data were imaged with DIFMAP (Shepherd, Pearson, & Taylor 1994) using cycles of deconvolution and selfcalibration.

## 3. RESULTS

In Figure 2 we present the naturally weighted images for the 102 CJ2 sources. While the lowest contour  $(3 \sigma)$  may be

<sup>&</sup>lt;sup>1</sup> The National Radio Astronomy Observatory is operated by Associated Universities, Inc., under cooperative agreement with the National Science Foundation.

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Telescope	Code	Location	Diam	$T_{\rm sys}$	T <sub>sys</sub>	Sensitivity
			(m)	(K)	(Jy)	(K/Jy)
(1)	(2)	(3)	(4)	(5)	(6)	(7)
Jodrell MKII	J2	Jodrell Bank, UK	26	45	375	0.12
Effelsberg	В	Germany	100	<b>58</b>	39	1.5
Onsala	$\mathbf{S}$	Sweden	26	58	983	0.059
WSRT	W	Netherlands	$5{\times}25$	64	128	0.5
Medicina	$\mathbf{L}$	Bologna, Italy	32	44	275	0.16
Noto	Ν	Noto, Italy	32	30	183	0.164
Simeiz	U	Crimea, Ukraine	22	103	3433	0.030
VLA <sup>a</sup>	Y	New Mexico, USA	<b>25</b>	57	491	0.116
VLBA_BR	$\mathbf{BR}$	Brewster WA, USA	<b>25</b>	33	282	0.117
VLBA_HN	HN	Hancock NH, USA	25	38	309	0.123
VLBA_NL	NL	North Liberty IA, USA	<b>25</b>	39	390	0.100
VLBA_OV	OV	Owens Valley CA, USA	25	38	302	0.126
VLBA_PT	$\mathbf{PT}$	Pie Town NM, USA	<b>25</b>	45	308	0.146

 TABLE 1

 Telescope Characteristics

NOTES.—Cols. (1)-(3): The name, the code used, and the location of each telescope. Affiliations: B, Max-Planck-Institüt für Radioastronomie; S, Onsala Space Observatory; W, Westerbork Synthesis Radio Telescope, NFRA; J2, Nuffield Radio Astronomy Laboratories; U, Space Research Institute, Moscow; L, N, Istituto di Radioastronomia; BR, HN, NL, OV, PT, National Radio Astronomy Observatory VLBA; Y, National Radio Astronomy Observatory VLA. Col. (4): The diameter of each telescope (in meters). Cols. (5)–(7): The system temperature in kelvins and in janskys and the sensitivity in kelvins per jansky of each telescope.

<sup>a</sup> The VLA was used in single antenna mode.

affected by residual systematic phase and amplitude errors, the second contour is reliable. The typical dynamic range, estimated as the ratio of the peak intensity to the rms in a blank area of sky, is  $\sim$  500:1, the same as that for the first three sessions. Fringe-fitting and mapping proved difficult for only one source, 1545+497, which was barely detected on the shortest baselines. Any derived parameters for this source must be interpreted with caution. Another source, 0256+424, was initially weak because the original position given by Patnaik et al.

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FIG. 1.—Typical *u-v* coverage for a source (1321+410) observed in the 1993 June session. The pattern is the result of three observations of 20 minutes each spaced over a wide range in hour angle.

(1992) and reproduced in Table 1 of Paper I was incorrect. This source was recorrelated at the correct position of  $\alpha(J2000) = 02^{h}59^{m}37.6753, \delta(J2000) = 42^{\circ}35'49''.9079.$ 

Tapered images are shown in cases where they reveal additional information. These were produced by using a Gaussian taper falling to 50% at 70 M $\lambda$  on the naturally weighted selfcalibrated data. All tapered images were restored with a circular 3 mas beam. The beam dimensions, rms, peak intensity, and lowest contour level (at 3  $\sigma$ ) for both the naturally weighted and tapered maps are shown in Table 2.

Model fitting was performed on the self-calibrated amplitudes and phases of each source in order to extract quantitative information, with up to four Gaussian components being fitted to each source. Model fitting was successful (total agreement factor < 1.2) for all 102 sources, and the model components are listed for each source in Table 3. The average total agreement factor is 1.004, slightly better than the value of 1.045 obtained for the previous three sessions. A description of the agreement factors is given in the Appendix.

## 4. SPECTRA

Integrated radio spectra for the entire CJ2 sample, covering the frequency range 151 MHz to 90 GHz, are given in Figure 3. These were compiled from various flux density catalogs in the literature, which are listed in Table 4. All the flux densities are on the absolute scale defined by Laing & Peacock (1980, hereafter LP),<sup>2</sup> and where necessary the original flux densities were converted to this scale, using correction factors that had already been determined by previous workers.

<sup>2</sup> The LP scale is identical to that of Baars et al. (1977) above 408 MHz (Riley 1988), and we have taken it to be identical above 327 MHz. At lower frequencies (178 MHz and below) the LP scale follows that of Roger, Bridle, & Costain (1973). Note that at 151 MHz the Baars et al. scale is  $\sim$ 0.95 times the LP scale.

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FIG. 2.—The 6 cm VLBI images for 102 sources in the CJ2 sample. Maps in which the epoch of observation is given in the upper right-hand corner are naturally weighted images, while those which are "tapered" have been weighted by a Gaussian taper and restored with a 3 mas beam as described in the text. The FWHM contour of the Gaussian beam is given in the lower left-hand corner and is listed in Table 2, along with the rms, peak intensity, and lowest contour level at 3  $\sigma$ . Contours are logarithmic at  $-3 \sigma$ , 3  $\sigma$ , 6  $\sigma$ , 12  $\sigma$ , etc. Negative contours are shown as dashed lines. FITS images corresponding to the maps presented in Fig. 2 are published in the AAS CD-ROM Series, Vol. 4.

![](_page_3_Figure_0.jpeg)

 $\ensuremath{\textcircled{}^{\odot}}$  American Astronomical Society  $\ \bullet$  Provided by the NASA Astrophysics Data System

![](_page_4_Figure_0.jpeg)

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![](_page_6_Figure_0.jpeg)

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![](_page_7_Figure_0.jpeg)

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![](_page_12_Figure_0.jpeg)

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![](_page_13_Figure_0.jpeg)

FIG. 2—Continued

1995ApJS..100...1H

TABLE 2Map Parameters

Name	Dur.		Beam		$S_{ m nat}$	rms	1st Cntr	$S_{\mathrm{tap}}$	$\mathbf{rms}$	1st Cntr
		a	ь	θ						
	(min)	(mas)	(mas)	(°)	(mJy/	beam)	(%Peak)	(mJy/	beam)	(%Peak)
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)
0003+380	57	2.17	0.92	-6	471	0.71	0.45			
0035 + 413	62	2.24	0.92	3	530	0.61	0.35	869	0.63	0.20
0100+351	57	2.80	0.85	_1	330	0.56	0.50	000	0.00	0.20
0103-001	57	1.61	0.00	-4	622	0.00	0.00			
0110+495	57	1.01	0.90	0	033	0.70	0.35			
0129 + 431	57	1.92	0.94	-8	275	0.40	0.45			
			0.01				0.00			
0145 + 386	57	2.21	0.91	-6	288	0.59	0.60			
0151 + 474	81	1.72	0.94	-4	723	0.55	0.25			
0201 + 365	76	2.66	0.82	-5	134	0.46	1.05			
0227 + 403	57	2.22	0.91	-6	459	0.66	0.45			
0249+383	57	2.27	0.89	-6	200	0.62	0.95			
0251 + 393	56	2.19	0.92	-4	410	0.44	0.30			
0256 + 424	59	1 93	0.88	_9	93	0 74	2 40	118	1.21	3.10
0307-380	95	2 41	0.00	ň	400	0.41	0.25	110	1.21	0.10
0200 + 411	76	2.41	0.00	0	210	0.41	0.20			
0309+411	70	2.14	0.90	0	319	0.40	0.40	507	0 50	0.20
0340+302	10	2.30	0.00	-3	440	0.41	0.50	327	0.52	0.50
0000 + 440		1 00	1	~1		0 70	1 80	0.10		
0600 + 442	57	1.88	1.04	-21	141	0.79	1.70	240	1.11	1.40
0627 + 532	76	1.79	0.98	<b>20</b>	152	0.63	1.25			
0641+393	76	2.41	0.90	0	495	0.45	0.25			
0650+453	57	1.68	1.03	2	415	0.57	0.40			
0651 + 410	57	1.97	0.95	-9	257	0.62	0.70			
$0700 + 470 \dots$	96	1.70	1.09	3	159	0.49	0.90	268	0.63	0.70
$0714 \pm 457$	57	1 72	0.00	-8	421	0.43	0.30	-00	0.00	0110
0797 + 400	57	2.02	0.00	-12	228	0.64	0.00	364	0.76	0.65
0721 + 409	57	1.61	1.00	-12	200	0.04	0.50	004	0.70	0.05
0731 + 479	57	1.01	1.00	-0	441 650	0.47	0.00			
0738 + 491	57	1.40	1.07	-2	059	0.37	0.15			
				_						
0739+398	76	2.37	0.91	-5	<b>214</b>	0.48	0.65	262	0.58	0.65
0743 + 744	57	1.21	1.01	22	327	0.59	0.55	416	0.83	0.60
0803 + 452	57	1.89	0.95	-5	<b>230</b>	0.46	0.60			
0824 + 355	56	2.39	0.94	-7	400	0.42	0.30	512	0.58	0.35
0830+425	56	1.84	1.00	0	264	0.55	0.65	300	0.61	0.60
0833+416	57	2.38	0.92	-8	195	0.61	0.95			
0902+490	58	1.73	0.98	-13	472	0.62	0.40			
0002 + 100	57	2 26	0.00	-6	235	0.67	0.85			
0025+504	07	1 60	1.07	26	0/0	0.57	0.00	1020	1.02	0.30
0920-004	57	2.00	0.05	-20	242	0.02	0.10	1020	1.02	0.50
0927+352	ុ១៸	2.50	0.95	-0	223	0.70	0.95			
0090 + 402		1.05	1.01	00	000	0.60	0 70			
0930+493	57	1.65	1.01	-23	293	0.69	0.70			
0933+503	57	1.84	0.96	-7	136	0.62	1.35	0.11	0 - 1	~ ~~
0941 + 522	57	1.56	1.03	-1	293	0.43	0.45	341	0.54	0.50
0942 + 468	55	1.48	1.13	-6	220	0.78	1.05			
0949 + 354	57	2.67	0.90	-4	273	0.55	0.60			
1010+350	58	2.45	0.88	-9	227	0.56	0.75			
1030+398	57	2.33	0.90	-8	432	0.50	0.35			
1038 + 528.	57	1.56	1.01	-6	639	0.55	0.25			
$1041 \pm 536$	58	1 48	1.03	5	264	0.43	0.50			
1041 + 000 $1105 \pm 437$	57	1 02	0.06	_2	254	0.10	0.50	280	0 50	0.55
1100-401		1.34	0.30		204	0.40	0.00	200	0.00	0.00
1194 + 455	57	0 1E	0.01	10	210	0 70	1 00			
1124+400	01 F <b>F</b>	2.10	0.91	-12	210	0.70	1.00	000	1 00	0.00
1144+352	57	2.50	0.90	-7	250	0.49	0.60	329	1.00	0.90
1146 + 531	57	1.49	1.00	-17	353	0.45	0.40	370	0.58	0.45
1151 + 408	57	2.25	0.90	-6	200	0.50	0.75	423	0.57	0.40
1155 + 486	57	1.55	1.08	-20	294	0.55	0.55	324	0.65	0.60
1205 + 544	57	1.47	1.13	-13	197	0.80	1.20			
1206 + 415	57	2.07	0.91	-5	286	0.58	0.60			
1221+809	57	1.13	1.03	57	239	0.44	0.55	297	0.65	0.65
1223 + 395	56	2.21	0.93	0	195	0.65	1.00	211	0.84	1.20
$1226 \pm 373$	57	2.35	0.92	_ <b>6</b>	693	0.49	0.20	723	0.50	0.20
10001010		2.00	0.04	0	300		0.20		0.00	0.20

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TABLE 2—Continued

Name	Dur.		Beam		$S_{\mathrm{nat}}$	$\mathbf{rms}$	1st Cntr	$S_{\mathrm{tap}}$	$\mathbf{rms}$	1st Cntr
		a	ь	θ						
	(min)	(mas)	(mas)	(°)	(mJy/	beam)	(%Peak)	(mJy/	beam)	(%Peak)
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)
1230+376	57	1 97	1.07	-5	208	0.69	1.00			
1260 + 381	57	2 20	0.05	_0	355	0.55	0.45	480	0.64	0.40
$1250\pm 532$	57	1 44	1 02	-10	181	0.50	0.15	100	0.04	0.40
1250 + 502	57	1.56	1.02	-10	219	0.00	0.05			
$1200 + 307 \dots$	57	1.00	0.07	14	210	0.70	0.90			
1300+4/1	57	1.01	0.97	-14	209	0.40	0.00			
1910   599	57	1 771	0.00	91	202	0 59	0.55			
$1312 + 333 \dots$	57	2.00	0.99	-01	101	0.02	1.05			
1321 + 410	57	2.00	0.97	-21	101	0.03	1.05			
1320 + 430	70	1.99	0.93	-19	3/1	0.48	0.40			
1413+373	76	2.45	0.92	-12	224	0.54	0.70			
1415 + 463	57	1.85	0.93	-16	234	0.67	0.85			
1 41 5 4 005		0.05	0.00		<b>F</b> 00	0 50	0.00			
1417 + 385	57	2.25	0.88	-11	560	0.56	0.30			
1421 + 482	57	1.83	0.91	-16	287	0.56	0.60			
1424 + 366	76	2.36	0:90	-13	627	0.45	0.20	719	0.60	0.25
1427 + 543	57	1.52	0.98	-28	<b>340</b>	0.61	0.55	410	0.76	0.55
1448 + 762	57	1.20	1.00	-79	300	0.50	0.50			
1456 + 375	57	2.32	0.88	-13	698	0.55	0.25			
1459 + 480	57	1.76	0.98	-39	392	0.71	0.55	433	1.15	0.80
1505 + 428	57	1.92	0.92	-16	309	0.53	0.50			
1534 + 501	76	1.76	0.93	-22	226	0.53	0.70			
1543 + 480	57	1.85	0.90	-14	283	0.50	0.55			
1543 + 517	76	1.53	0.96	-17	404	0.46	0.35	479	0.56	0.35
1545 + 497	57	1.55	0.98	-25	<b>24</b>	0.43	5.40			
1550 + 582	57	1.43	0.95	-31	211	0.49	0.70			
1602 + 576	57	1.45	0.96	-18	212	0.63	0.90			
1619+491	57	1.70	0.95	-22	211	0.45	0.65	282	0.58	0.60
1629 + 495	57	1.77	0.92	-26	366	0.67	0.55			
1636 + 473	57	1.92	0.92	-28	547	0.78	0.45			
1638 + 540	76	1.36	1.03	-20	171	0.48	0.85			
1645 + 410	57	2.33	0.89	-14	497	0.56	0.35			
1722 + 401	57	2.00	0.94	-14	283	0.57	0.60	319	0.83	0.80
	•••		0.01					010	0.00	0.00
1726+455	57	1.83	0.92	-14	1080	0.82	0.25			
1734 + 363	57	2 59	0.88	-15	392	0.55	0.40			
$1742 \pm 402$	57	3.69	1 20	_9	139	0.79	1 70	182	0.90	1 50
$1747 \pm 433$	95	2.05	0.91	_7	262	0.39	0.45	269	0.53	0.60
$1819 \pm 419$	57	2.00	0.01	_10	256	0.52	0.10	272	0.84	0.00
10101 112	01	<b>2.11</b>	0.01	10	200	0.04	0.00	212	0.04	0.00
$1828 \pm 399$	76	2 40	0.84	-13	213	0.45	0.65			
1830-380	76	2.40	0.04	_19	204	0.10	0.00			
1950   402	59	2.01	0.00	15	204	0.42	1.05			
1030 + 402	57	2.02	0.92	0	244	0.00	1.00	340	0.61	0 50
1015 657	76	1.20	1.02	<i>3</i> 52	941	0.43	0.50	043	0.01	0.00
1910-001	10	1.24	1.00	00	241	0.40	0.00			
1024+507	76	1 35	1.05	_13	280	0.58	0.60	3/1	0.84	0.75
1324TUUI	10	1.00	1.00	-13	409	0.00	1 05	041	0.04	0.10
2010-000	07 07	⊿.04 ე_∩∩	0.90	-0 19	104 105	0.00	1.00			
<b>∠</b> 319+444	91	2.09	0.00	-13	490	0.00	0.30	049	0 79	0.00
233U+38(	58 57	⊿. <b>3</b> 0	0.89	-12	119	0.40	0.70	243	0.13	0.90
<b>2340+38</b> 5	57	2.34	0.88	-12	592	0.98	0.30			
0256 L 205	70	0 70	0.05	7	949	0.47	0.60			
<b>∠</b> JJU+J8J	(0	4.12	0.00	-1	243	0.41	0.00	044	0.49	0.00
∠300+390	70	2.58	0.85	-10	212	0.44	0.00	244	0.48	0.60

NOTES.—Col. (2): Total integration time on source in minutes. Cols. (3)–(5): The beam characteristics of the naturally weighted maps. The restoring beam is an elliptical Gaussian with FWHM major axis *a* mas and minor axis *b* mas, with major axis in position angle  $\theta^{\circ}$ . Col. (6): The peak intensity of the naturally weighted maps (mJy beam<sup>-1</sup>). Col. (7): The rms noise in the naturally weighted maps (mJy beam<sup>-1</sup>), measured in the four corners of the displayed image. Col. (8): The lowest contour level of the map in percentage of the peak flux density. Cols. (9)–(11): The peak intensity, rms noise, and lowest contour level of the tapered map, if an image has been provided. All tapered maps have been restored with a 3 mas beam.

Table 2 is published in computer-readable form in the AAS CD-ROM Series, Vol. 4.

995ApJS100	.1H	
995ApJS100	•	
995ApJS100.	•	
995ApJS100	•	
995ApJS10	0	
995ApJS1	0	
995ApJS		-
995ApJS.	•	
	995ApJS.	

					TAB	LE 3				
_					GAUSSIAN	MODE	LS			
	Source	$S \ (Jy)$	$r \pmod{(\mathrm{mas})}$	<i>θ</i> (°)	$a \pmod{(\max)}$	b/a	Φ (°)	Amplitude A.F.	Cl.Phase A.F.	Total A.F.
	0003+380	0.526	0.00	0.0	0.69	0.46	114.4	1.000	1.063	1.028
		0.183	0.89	122.4	0.61	0.14	146.2			
		0.013	4.62	111.9	1.67	0.53	7.4			
	0095 1 419	0.456	0.00	0.0	0.57	0.00	00.1	1 094	1 154	1 094
	0035+415	0.450	0.00	0.0 95.8	0.57	0.00	99.1 	1.024	1.104	1.084
		0.017	3.80	101.8	1.46	0.00	23.3			
		0.067	9.62	112.9	10.14	0.29	127.0			
	$0109 + 351 \dots$	0.300	0.00	0.0	0.45	0.00	-155.9	1.025	1.042	1.033
		0.065	0.58	-163.9	0.96	0.26	-150.3			
		0.014	5.54	-156.3	7.00	0.09	-155.8			
	0110	0.666	0.00	0.0	0.67	0.23	-27.8	1 012	1 003	1 0/0
	01107495	0.000	1.05	-39.8	2.78	0.23	-27.0 -37.4	1.012	1.035	1.045
		0.094	8.33	-30.9	4.11	0.46	0.1			
	0129+431	0.289	0.00	0.0	0.49	0.39	159.5	1.001	1.022	1.010
		0.013	1.95	-7.5	3.11	0.16	28.9			
	0145 . 000	0 401	0.00	0.0	0.05	0.01	100.1	0.015	1 1 5 0	1 000
	$0145 + 386 \dots$	0.401	0.00	0.0	0.95	0.01	122.1	0.917	1.153	1.030
		0.057	1.16	-43.5	0.65	0.52	23.0			
	0151+474	0.762	0.00	0.0	0.43	0.51	16.3	0.876	1.012	0.939
		0.036	1.67	-178.6	0.76	0.54	-3.8			
	$0201 + 365 \dots$	0.144	0.00	0.0	0.34	0.59	45.7	1.016	1.165	1.085
		0.108	2.45	-3.5	1.03	0.45	-11.7			
		0.035	7.24	-3.8	3.54	0.60	4.9			
	0227-1403	0 502	0.00	0.0	0.75	0.30	162 1	0.050	1.053	0.007
	0221   400	0.048	2.38	138.6	2.63	0.10	120.8	0.500	1.000	0.001
		0.010	2.00	20010	2.00	0.20	12010			
	0249+383	0.199	0.00	0.0	0.61	0.86	165.1	1.050	1.042	1.047
		0.107	1.47	-12.8	2.01	0.37	-31.1			
		0.056	5.15	-19.7	3.44	0.33	-28.7			
	0251.1 202	0.438	0.00	0.0	0 /3	0.35	00.0	0.077	1.016	0.004
	$0201 + 355 \dots$	0.438	0.00	80.6	1 20	0.33	50.9 10.2	0.917	1.010	0.334
		0.008	9.13	65.1	1.40	0.00	48.8			
	$0256 + 424 \dots$	0.113	0.00	0.0	0.74	0.00	35.0	1.040	1.244	1.135
		0.151	10.34	65.4	1.39	0.60	-51.8			
		0.106	4.57	55.7	1.74	0.46	-86.9			
	0307-1380	0 515	0.00	0.0	0 32	0.44	80.2	0.015	1 002	0.055
	03017300	0.006	3.57	68.7	0.80	0.44	47.7	0.910	1.002	0.300
			0.01							
	0309+411	0.318	0.00	0.0	0.44	0.82	135.9	0.895	1.029	0.957
		0.112	0.91	-51.5	1.19	0.00	-62.8			
		0.031	3.74	-55.2	3.26	0.00	-61.7			
	0340-1-363	0.470	0.00	0.0	0 52	0 55	510	0 006	1 020	0.063
	0340+302	0.470	0.00	31.8	0.55	0.55	04.0 80.8	0.890	1.059	0.905
		0.001	9.52	21.0	4.28	0.18	145.1			
	$0600 + 442 \dots$	0.222	0.00	0.0	1.08	0.70	-69.4	1.027	1.211	1.112
		0.159	2.52	-49.6	2.44	0.75	-26.6			
		0.080	5.04	-35.3	5.38	0.67	12.3			
	0697 1 599	0.915	0.00	0.0	1 01	0.02	er c	1 049	1 1 4 6	1 000
	00217032	0.210	2.81	-132 1	0.77	0.23	-160 1	1.043	1.140	1.090
		0.151	2.68	66.7	2.27	0.33	48.9			
		0.026	8.94	52.1	3.01	0.36	46.6			

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TABLE 3—Continued											
Source	$S \ (Jy)$	r (mas)	θ (°)	a (mas)	b/a	ф (°)	Amplitude A.F.	Cl.Phase A.F.	Total A.F.		
0641+393	0.498	0.00	0.0	0.42	0.40	19.1	0.902	1.026	0.960		
	0.063	1.77	-7.4	4.02	0.21	-1.6					
	0.016	4.70	1.4	3.05	0.13	32.1					
0650+453	0.431	0.00	0.0	0.29	0.73	135.5	0.901	1.037	0.965		
	0.037	1.04	100.1	2.17	0.39	53.2					
0651+410	0.308	0.00	0.0	1.12	0.27	166.0	0.866	1 052	0 954		
	0.033	1.56	156.4	0.79	0.00	72.4		1.002	0.001		
0700+470	0.280	0.00	0.0	1.59	0 44	-24.2	1 084	1 310	1 188		
	0.123	2.44	122.6	2.71	0.34	102.2	1.001	1.010	1.100		
	0.098	7.05	93.1	6.16	0.34	64.2					
	0.012	21.21	77.9	7.32	0.00	138.8					
0714+457	0.424	0.00	0.0	0.41	0.08	148.7	0.909	1.047	0.974		
	0.095	2.02	124.8	4.66	0.17	127.2					
	0.005	17.46	117.5	1.48	0.24	23.0					
0727+409	0.213	0.00	0.0	0.49	0.57	-44.8	1.024	1.203	1.106		
	0.197	1.12	124.1	0.74	0.44	139.3					
	0.007	2.89	-51.9	0.02	0.91	35.4					
0731+479	0.231	0.00	0.0	0.37	0.72	61.1	1.009	1.063	1.034		
	0.182	1.02	-103.6	0.84	0.34	-83.3					
	0.093	2.40	-87.9	1.87	0.08	-98.3					
	0.006	8.86	-85.7	1.01	0.38	-16.9					
0738+491	0.691	0.00	0.0	0.28	0.94	174.1	0.879	1.009	0.939		
0739+398	0.209	0.00	0.0	0.76	0.38	161.6	1.000	1.080	1.037		
	0.103	1.53 5.88	158.2 140.6	0.70	0.52	142.5 120.9					
	0.000	0.00	110.0	0.01	0.20	120.0					
0743+744	0.368	0.00	0.0	0.71	0.20	24.8	0.891	1.064	0.972		
	0.031	5.32	28.0 28.5	1.88	0.33	-17.9 127.9					
0803+452	0.374	$0.00 \\ 2.03$	0.0 -123.6	1.26	0.28 0.55	-125.8 125.4	0.997	1.207	1.096		
	01000	2.00	12010	0.00	0.00						
0824+355	0.528	0.00	0.0	0.79	0.31	100.2	0.916	1.144	1.024		
	0.131	11.07	02.0	22.05	0.19	52.7					
0830+425	0.299	0.00	0.0	0.57	0.41	-74.9	0.994	1.040	1.015		
	0.034	3.72	-84.1	6.02	0.00	-86.8					
0833+416	0.238	0.00	0.0	1.41	0.24	5.0	0.987	1.162	1.069		
·	0.083	2.12	-171.9	0.44	0.05	-28.0					
0902+490	0.480	0.00	0.0	0.39	0.76	-32.6	0 940	1 065	0 998		
	0.141	1.18	-39.8	0.76	0.95	-37.8	010 10	1.000	0.000		
0010 - 001	0.050	0.00				00.0	0.045	1 000	1.011		
$0913 + 391 \dots$	0.276	0.00	0.0	0.74	0.77	28.0	0.945	1.088	1.011		
	0.120	2.32	-114.9 -07.0	1.00	0.87	9.11 20.1					
	0.135	0.07	-31.3	1.15	0.14	23.1					
$0925 + 504 \dots$	1.032	0.00	0.0	0.51	0.36	107.2	0.918	1.029	0.969		
	0.035	5.24	126.4	7.65	0.24	128.5					
0927+352	0.242	0.00	0.0	0.49	0.69	138.9	1.038	1.079	1.056		
	0.078	4.36	103.0	3.95	0.43	102.1			-		
0930+493	በ 483	0.00	0.0	1 17	0.55	-133.6	ሀ ያዊያ	1 1 9 9	0.085		
00001300	0.076	2.57	-136.3	1.12	0.30	-143.1	0.000	1.144	0.000		

			TA	BLE 3—	Continu	ed			
Source	$rac{S}{(\mathrm{Jy})}$	$r \ ({ m mas})$	<i>θ</i> (°)	a (mas)	b/a	Φ (°)	Amplitude A.F.	Cl.Phase A.F.	Total A.F.
0933+503	0.127	0.00	0.0	0.06	0.00	127.2	0.972	1.079	1.021
	0.065	0.92	64.0	0.92	0.43	58.4			
0941+522	0.350	0.00	0.0	0.80	0.44	165.8	0.975	1.117	1.041
	0.122	3.50	150.8	1.21	0.65	166.4			
	0.074	5.82	163.9	6.45	0.13	158.0			
	0.009	30.82	175.4	1.57	0.00	118.0			
0942+468	0.229	0.00	0.0	0.59	0.50	62.1	0.981	1.068	1.021
	0.075	1.01	47.4	0.68	0.56	14.8			
	0.049	2.62	31.1	1.94	0.71	72.0			
0949+354	0.296	0.00	0.0	0.99	0.27	168.9	0.988	1.164	1.071
	0.078	3.11	167.0	5.11	0.13	169.9			
1010+350	0.233	0.00	0.0	0.26	0.57	50.6	0.876	1.003	0.935
	0.088	1.83	98.0	1.22	0.70	32.0			
	0.033	5.40	99.1	4.47	0.22	78.6			
1030+398	0.577	0.00	0.0	1.10	0.13	35.0	0.907	1.090	0.994
	0.108	2.04	47.6	0.95	0.33	87.4			
	0.007	7.58	40.9	0.61	0.00	65.1			
038+528	0.667	0.00	0.0	0.48	0.12	16.2	0.906	1.063	0.979
	0.055	1.25	27.1	0.16	0.17	132.8			
	0.027	2.71	18.3	3.88	0.24	27.4			
.041+536	0.346	0.00	0.0	0.97	0.33	145.3	0.996	1.045	1.019
	0.053	2.58	160.1	3.28	0.34	178.7			
1105+437	0.246	0.00	0.0	0.26	0.00	-133.5	1.000	1.049	1.022
	0.055	0.98	-136.5	1.45	0.47	-138.7			
	0.012	8.66	-125.6	3.27	0.29	-26.3			
$124 + 455 \dots$	0.213	0.00	0.0	0.81	0.00	-25.5	1.009	1.195	1.096
	0.145	2.48	-5.0	2.37	0.12	0.5			
1144+352	0.297	0.00	0.0	0.60	0.86	31.9	0.962	1.159	1.055
	0.170	2.66	-58.2	3.99	0.86	-55.3			
	0.071	21.67	-58.5	0.55	0.78	-49.2			
1146+531	0.378	0.00	0.0	0.37	0.70	122.4	0.884	1.046	0.960
$1151 + 408 \dots$	0.365	0.00	0.0	1.08	0.83	64.3	0.919	1.184	1.047
	0.181	1.66	73.1	0.92	0.00	88.3			· •
1155+486	0.310	0.00	0.0	0.46	0.40	-78.7	0.889	1.068	0.972
	0.041	1.53	-100.5	2.40	0.31	-132.0			
1205+544	0.284	0.00	0.0	1.00	0.63	105.6	0.949	1.153	1.045
	0.141	2.48	121.5	0.91	0.32	58.2			
1206+415	0.327	0.00	0.0	0.53	0.68	40.5	0.903	1.019	0.957
	0.007	16.36	-162.8	0.63	0.00	-54.7			
221+809	0.239	0.00	0.0	0.33	0.33	-22.2	0.887	1.036	0.956
	0.074	1.02	-3.5	0.65	0.63	-19.1			
	0.093	6.12	-6.6	6.06	0.18	-11.7			
.223+395	0.206	0.00	0.0	0.56	0.41	18.6	0.906	1.188	1.041
	0.016	3.22	35.6	3.01	0.35	14.6			
	0.217	7.55	34.7	1.34	0.43	8.1			
	0.067	12.64	27.0	6.51	0.26	46.0			

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			TA	ABLE 3-	-Contin	ued			
Source	S (Jy)	r (mas)	θ (°)	a (mas)	b/a	Φ (°)	Amplitude A.F.	Cl.Phase A.F.	Total A.F.
1226+373	0.729 0.012	0.00 3.17	0.0 -70.7	0.34 2.09	0.67 0.00	$-51.4 \\ -127.9$	0.886	1.014	0.946
1239+376	0.231 0.189	$0.00 \\ 1.54$	0.0 -159.8	1.51 0.80	0.34 0.78	2.3 107.7	0.863	1.100	0.974
1240+381	0.526	0.00	0.0	1.08	0.45	-66.3	0.892	1.106	0.994
$1250 + 532 \dots$	$0.207 \\ 0.063$	0.00 4.28	$\begin{array}{c} 0.0 \\ -100.4 \end{array}$	$0.59 \\ 5.53$	0.19 0.24	$\begin{array}{c} -120.1 \\ -96.4 \end{array}$	0.922	1.073	0.992
1258+507	0.194 0.152	$0.00 \\ 1.30$	0.0 162.9	0.20 0.63	$0.83 \\ 0.50$	$82.9 \\ 159.8$	0.887	1.110	0.992
1308+471	0.256	0.00	0.0	0.38	0.72	24.6	0.851	1.038	0.939
1312+533	$0.300 \\ 0.170$	$0.00 \\ 1.53$	0.0 -118.4	$0.27 \\ 1.01$	$0.80 \\ 0.47$	$1.5 \\ -110.8$	0.863	1.047	0.950
1321+410	0.226	0.00	0.0	0.62	0.93	-90.9	0.865	1.194	1.022
$1325 + 436 \dots$	0.187 0.403	5.42 0.00	-82.5 0.0	0.74 0.75	0.85 0.43	20.1 40.4	0.896	1.118	1.001
	0.181	0.78	-139.0	0.85	0.92	-173.3			1.001
1413+373	0.263 0.096 0.023	$     \begin{array}{r}       0.00 \\       1.56 \\       1.65     \end{array} $	-44.7 116.9	0.77 0.23 0.72	0.15 0.00 0.26	$   \begin{array}{r}     109.9 \\     -1.0 \\     21.2   \end{array} $	0.889	1.088	0.983
1415+463	0.010 0.234	4.25 0.00	116.5 0.0	0.54 0.41	0.01 0.82	29.7 46.9	0.901	1.125	1.007
	$0.232 \\ 0.043 \\ 0.155$	1.14 2.53 10 47	76.2 -95.3 -97.5	$1.02 \\ 1.12 \\ 0.84$	$0.00 \\ 0.59 \\ 0.73$	87.0 3.3 54.4			
417+385	0.619	0.00	0.0	0.41	0.92	-10.7	0.972	1.036	1.001
421+482	0.324 0.074	$\begin{array}{c} 0.00\\ 2.24 \end{array}$	0.0 -73.0	$0.52 \\ 2.62$	0.75 0.64	$-100.0 \\ -72.9$	0.864	1.087	0.971
424+366	0.669 0.090	$0.00 \\ 1.13$	$0.0 \\ -129.6$	0.40 0.52	0.71 0.00	27.2 - 37.7	0.874	1.036	0.950
427+543	0.351	0.00	0.0	0.58	0.37	138.4	0.941	1.043	0.987
	0.100	6.20	141.5	0.76 7.43	0.34 0.16	119.9			
448+762	0.318 0.088	0.00 0.77	0.0 81.5	$\begin{array}{c} 0.66\\ 1.08\end{array}$	0.19 0.43	78.5 82.8	0.845	1.063	0.947
456+375	0.737 0.045	0.00 1.36	$\begin{array}{c} 0.0\\112.8\end{array}$	0.30 1.42	$\begin{array}{c} 0.98 \\ 0.56 \end{array}$	168.9 9.4	0.900	1.077	0.983
459+480	0.400 0.067	0.00 1.43	0.0 86.0	$0.36 \\ 1.74$	0.25 0.19	40.4 82.0	0.870	1.066	0.962
505+428	0.059	6.66 0.00	72.9	5.97 0.62	0.10 0.54	50.4 	0 802	1 058	0 970
1000   120	0.042 0.037	$1.17 \\ 5.00$	$-97.8 \\ -103.8$	$\begin{array}{c} 0.02\\ 0.00\\ 4.35\end{array}$	0.70 0.00	-95.2 -109.0	0.074	1.000	0.310
534+501	0.315	0.00	0.0	1.43	0.13	-35.4	0.947	1.277	1.108

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1H				TA	ABLE 3-	-Contin	ued			
.100.	Source	S (Jy)	r (mas)	θ (°)	a (mas)	b/a	Φ (°)	Amplitude A.F.	Cl.Phase A.F.	Total A.F.
pJS.	1543+480	0.299 0.116	0.00	0.0 141.3	0.46 1.23	0.80 0.54	97.8 141.9	0.914	1.051	0.978
995A		0.079	34.93	115.6	0.68	0.93	63.6			
-1	1543+517	$0.358 \\ 0.131$	0.00 0.74	0.0 173.2	0.42	0.52 0.33	177.9 57.0	0.893	1.044	0.964
		0.055	2.26	-169.4	1.15	0.50	23.4			
		0.022	5.34	179.4	1.19	0.62	120.3			
		0.057	23.39	172.1	8.21	0.24	149.9			
	1545+497	0.041	0.00	0.0	0.44	0.30	37.1	0.876	1.141	1.002
	$1550 + 582 \dots$	0.195	0.00	0.0	0.49	0.23	160.5	0.847	1.026	0.931
		0.093	1.03	163.2	1.33	0.00	143.6			
	$1602 + 576 \dots$	0.278	0.00	0.0	0.92	0.34	140.1	0.902	1.086	0.988
		0.076	3.87	130.9	0.53	0.67	12.2			
	1619+491	0.236	0.00	0.0	0.66	0.40	5.7	0.892	1.075	0.978
		0.087	1.30	9.0	0.47	0.01	96.6			
		0.052	0.51 10.26	2.5 8.2	1.66	0.59	38.4 			
				0.2						
	$1629 + 495 \dots$	0.415	$0.00 \\ 1.12$	0.0 	0.53	0.31	-112.4 -8 1	0.890	1.050	0.965
		0.000	1.10	111.0	0.00	0.01	0.1			
	$1636 + 473 \ldots$	0.705	0.00	0.0	1.48	0.17	-20.7	1.048	1.086	1.065
		0.045	0.00	-31.3	0.99	0.15	-20.0			
	$1638 + 540 \dots$	0.229	0.00	0.0	0.79	0.72	-147.3	0.821	1.106	0.957
		0.000	1.22	-130.2	0.34	0.40	-31.9			
	1645+410	0.465	0.00	0.0	0.19	0.34	128.8	0.873	1.011	0.937
		0.085	0.89	130.1	0.81	0.00	98.8			
	1			0.0				0.040	4	1
	$1722 + 401 \dots$	0.336 0.055	0.00 4.41	$0.0 \\ -53.4$	0.73 2.88	0.52 0.44	131.7 44.6	0.949	1.078	1.009
		0.000		00.1	2.00	0.11	1110			
	$1726 + 455 \dots$	1.109	0.00	0.0 	0.32	0.98	-80.0	0.932	1.042	0.983
		0.150	0.50	10.0	0.52	0.02	14.0			
	1734+363	0.534	0.00	0.0	0.80	0.59	71.7	0.873	1.041	0.952
	$1742 + 402 \dots$	0.217	0.00	0.0	1.20	0.83	15.3	0.845	1.259	1.031
		0.116	4.77	-94.6	2.57	0.54	-89.3			
		0.053	11.04	-104.5	4.68	0.63	-90.2			
	$1747 + 433 \dots$	0.252	0.00	0.0	0.10	0.00	104.0	0.883	1.036	0.955
		0.022	0.94	-171.2	1.10	0.00	-16.1			
		0.011	3.40 13.29	167.1	2.35	0.70	$4.0 \\ 115.0$			
					o 44		100.0		1 000	o o <b>-</b> 4
	$1812 + 412 \dots$	0.275	0.00	0.0	0.41	0.83	138.0	0.881	1.038	0.954
		0.023	4.24 11 94	85.0 85.4	2.12 5.30	0.21	107.4			
		0.004	11.47	00.4	0.00	0.14	00.0			
	$1828 + 399 \dots$	0.222	0.00	0.0	0.44	0.79	-112.4	0.841	1.068	0.949
		0.072	0.98	-09.8	0.98	0.23	-02.0			
	1839+389	0.220	0.00	0.0	0.35	0.87	128.7	0.861	1.069	0.960
	1850+402	0.272	0.00	0.0	0.92	0.37	55.0	0.859	1.204	1.025
		0.376	1.41	61.8	1.64	0.19	69.2			

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			TAB	LE 3—C	ontinued	1			
Source	S	r	θ	a	b/a	Φ	Amplitude	Cl.Phase	Total
	(Jy)	(mas)	(°)	(mas)		(°)	A.F.	A.F.	A.F.
1910+375	0.388	0.00	0.0	1.33	0.25	159.8	0.892	1.045	0.964
	0.021	7.52	177.5	3.32	0.26	-49.5			
1015 + 657	0 206	0.00	0.0	0.62	0.79	91.1	0 000	1 069	0.079
1910-007	0.000	2.68	-54.4	2 56	0.16	11 1	0.898	1.008	0.910
	0.040	200		0.86	0.40	77			
	0.015	32.01	-111.8	0.00	0.00	1.1			
1924+507	0.301	0.00	0.0	0.50	0.23	1.0	0.878	1.017	0.943
	0.110	2.00	-0.4	1.26	0.26	1.9			
	0.011	8.41	3.0	3.11	0.38	77.2			
$2310 + 385 \dots$	0.296	0.00	0.0	1.21	0.36	-121.1	0.876	1.190	1.026
	0.070	1.57	-131.1	1.90	0.00	-167.9			
	0.145	4.39	59.2	1.36	0.46	50.1			
2319+444	0.509	0.00	0.0	0.26	0.61	2.5	0 873	1 007	0 935
1010   111   11	0.038	2.13	-16.5	0.70	0.39	-7.8	0.010	21001	0.000
	0.000		1010	0110	0.00				
2330+387	0.250	0.00	0.0	1.00	0.58	24.8	1.037	1.230	1.126
	0.033	1.68	-161.0	0.00	0.80	0.0			
	0.182	<b>45.20</b>	-151.9	4.44	0.49	-144.9			
1946 - 20E	0 691	0.00	0.0	0.44	0.99	17 9	0.005	1 090	0.060
23407303	0.021	1 01	0.0	0.44	0.23	-47.5	0.905	1.029	0.902
	0.034	1.91	-20.1	0.00	0.00	51.7			
2356+385	0.342	0.00	0.0	1.67	0.30	-21.4	0.893	1.232	1.059
	0.038	0.98	-136.4	0.826	0.00	31.5			
2356+390	0.214	0.00	0.0	0.26	0.93	51.1	0.916	1.073	0.990
	0.057	1.71	-129.2	1.07	0.31	-139.0			
	0.012	3.71	-128.9	0.64	0.00	-95.2			
	0.031	8.82	-134.9	4.14	0.83	-130.7			

NOTES.—Parameters of each Gaussian component of the model brightness distribution: S, flux density; r,  $\theta$ , polar coordinates of the center of the component relative to an arbitrary origin, with polar angle measured from north through east; a, b, major and minor axes (FWHM);  $\Phi$ , position angle of the major axis measured from north through east.

Table 3 is published in computer-readable form in the AAS CD-ROM Series, Vol. 4.

![](_page_22_Figure_1.jpeg)

FIG. 3.—Integrated radio spectra for the entire CJ2 sample. All flux densities are on the scale of Laing & Peacock (1980). The error bars are  $\pm 1 \sigma$  and are mainly taken from the flux density catalogs, although we have estimated some of these.

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![](_page_23_Figure_1.jpeg)

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![](_page_24_Figure_1.jpeg)

 $\ensuremath{\textcircled{}^{\odot}}$  American Astronomical Society • Provided by the NASA Astrophysics Data System

![](_page_25_Figure_0.jpeg)

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![](_page_26_Figure_1.jpeg)

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![](_page_27_Figure_0.jpeg)

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![](_page_28_Figure_1.jpeg)

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![](_page_29_Figure_1.jpeg)

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![](_page_30_Figure_1.jpeg)

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![](_page_31_Figure_0.jpeg)

![](_page_31_Figure_1.jpeg)

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![](_page_32_Figure_1.jpeg)

FIG. 3—Continued

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TABLE 4	
UX DENSITY CATALOGS	s

FLUX DENSITY CATALOGS				
Frequency (MHz)	Survey	Reference(s)	Typical Error	Correction Factor
(1)	(2)	(3)	(4)	(5)
151	6C	Baldwin et al. (1985),	50 mJy	_
		Hales, Baldwin & Warner (1988, 1993),		
		Hales et al. (1990, 1991, 1993)		
178	4C	Pilkington & Scott (1964),	10%	$1.09^{a}$
		Gower, Scott & Wills (1967)		
318		Kühr et al. (1979)	150 mJy	-
327	WENSS	WENSS team, 1994, priv. comm.	10%	-
365	Texas	Douglas et al. (1980)	15  mJy	$1.041^{b}$
408	B2.3	Colla et al. (1973)	50  mJy	$0.96 - 1.02^{c}$
408	<b>B3</b>	Ficarra et al. (1985)	50  mJy	$0.96 - 1.02^{c}$
610	VRO	Macleod et al. (1965)	20%	$1.065^{d}$
750		Pauliny-Toth, Wade & Heeschen (1966)	200 mJy	$1.059^{e}$
750		Owen, Spangler & Cotton (1980)	100 mJy	$1.035^{e}$
966		Kühr et al. (1979)		
968		Owen, Spangler & Cotton (1980)	100 mJy	$1.026^{e}$
1400		White & Becker (1992)	15%	-
2700		Kühr et al. (1979)	25  mJy	-
4585		Kühr et al. (1979)	40 mJy	_
4850	87GB	Gregory & Condon (1991)	15%	
4890	S5	Kühr et al. (1981a)	5  mJy	-
8400	JVAS	Patnaik et al. $(1992)$ and other	5%	-
		JVAS papers in preparation		
10700		Kühr et al. (1979)	25  mJy	_
15000		Owen, Spangler & Cotton (1980)	40 mJy	-
15064		Kühr et al. (1979)	80 mJy	-
22185		Kühr et al. (1979)	150 mJy	-
31400		Kühr et al. (1979)	90 mJy	-
31400		Owen, Spangler & Cotton (1980)	200 mJy	-
90000		Kühr et al. (1979)	160 mJy	-
90000		Owen, Spangler & Cotton (1980)	200 mJy	

NOTES.—Col. (1): The frequency of observation (in MHz). Col. (2): Name of the survey (if any); abbreviations are as follows: 6C, 6th Cambridge Survey; 4C, 4th Cambridge Survey; WENSS, Westerbork Northern Sky Survey; Texas, Texas Survey; B2.3, B3, Second Bologna Survey (Third Part) and Third Bologna Survey, respectively; VRO, Vermilion River Observatory Survey; 87GB, 1987 Green Bank Survey; S5, 5th Strong Source Survey; JVAS, Jodrell Bank – VLA Astrometric Survey. Col. (3): Reference(s) for the flux density catalog. A subsample of Kühr et al. 1979 containing only the sources stronger than 1 Jy at 5000 MHz was later published as Kühr et al. 1981b. Col. (4): Estimate of the typical uncertainty on the flux densities in the catalog, either in millijanskys or as a percentage of the flux density. Note that the error bars in Fig. 3 are taken predominantly from the uncertainties quoted for each flux densities in the catalog, rather than these estimated values. Col. (5): The correction factor applied to the flux densities in the catalog for correction factor: a, Roger, Bridle, & Costain 1973; b, J. Douglas, private communication; c, Riley 1988, correction factor depends on flux; d, Baars et al. 1977; e, Kühr et al. 1981b.

The flux density measurements for 1038+528 that were made with low-resolution instruments will be contaminated by a strong quasar, 1038+528B, located only 33'' to the northwest. VLBI observations of both quasars are reported by Marcaide & Shapiro (1984).

The spectral index distribution for the CJ2 sample is shown in Figure 4. Note that most flat-spectrum sources are variable, and since the flux density measurements at different frequencies were not simultaneous, the spectral indices derived are only representative and will differ from the instantaneous values. While the vast majority of the CJ2 sample have flat radio spectra, there are 13 "steep-spectrum" sources with  $\alpha < -0.5$ . Thus the CJ2 sample is not a perfect spectrally limited sample.

# 5. SUMMARY

Global VLBI images at 4992 MHz are presented for the 102 sources observed in the final observing session of the CJ2 survey. We also present integrated radio spectra for the entire CJ2 sample. Future papers will discuss the interpretation of these observations and of second-epoch observations. A concerted effort is underway to obtain redshifts for all objects in this sample.

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![](_page_34_Figure_2.jpeg)

FIG. 4.—Distribution of spectral index (defined as  $S_{\nu} \propto \nu^{\alpha}$ ) for the CJ2 sample. For most sources,  $\alpha$  has been calculated between 365 MHz and 8400 MHz (shown with no shading). For 49 sources, with unknown 365 MHz flux densities,  $\alpha$  has been calculated between 1400 MHz and 8400 MHz (*gray shading*); and for 12 sources, with both an unknown 365 MHz and 1400 MHz flux density,  $\alpha$  has been calculated between 4850 MHz and 8400 MHz (*black shading*). We thank the staff at the VLA, VLBA, and European VLBI Network observatories who took part in these observations and the staff of the JPL/Caltech Block II Correlator for their assistance. We also thank Sally Hales for help in obtaining the 151 MHz flux densities and for advice on the use of flux density scales. We are grateful to Jim Douglas for providing 365 MHz flux densities prior to publication and to Ger de Bruyn for providing 327 MHz flux densities from the WENSS prior to publication. We are indebted to Martin Shepherd for writing and maintaining DIFMAP and for the many modifications he made on our behalf. Thanks also to Roddy Calder for help with Figure 4. D. R. H. acknowledges the receipt of a SERC research studentship. The work done by the Caltech group was supported by the NSF under grant AST-9117100.

# APPENDIX AGREEMENT FACTORS

Table 3 lists *agreement factors* between the models and observed visibilities. Separate agreement factors are given for amplitude and closure phase. In addition a total agreement factor (a weighted average of the amplitude and closure-phase agreement factors) is given; this is the quantity that is minimized in the least-squares model-fitting procedure. The closure-phase agreement factor is useful because it is not affected by antenna phase calibration errors.

## A1. AMPLITUDE AGREEMENT FACTOR

Denoting the model amplitude and phase at a sample point by  $A_m$  and  $\phi_m$  and the observed amplitude and phase by  $A_0$  and  $\phi_0$  with standard errors  $\sigma_A$  and  $\sigma_{\phi}$ , the *amplitude agreement factor* is

$$Q_{\rm AMP} = \sqrt{\frac{1}{M} \sum_{1}^{M} \left(\frac{A_0 - A_m}{\sigma_A}\right)^2},\tag{1}$$

where the sum is over M measured visibility samples. Assuming that all the samples are independent and that the measured amplitudes have a Gaussian distribution (high-SNR approximation), the sum of squares in this expression is distributed as  $\chi^2$  with M degrees of freedom, and  $Q^2_{AMP}$  is a reduced  $\chi^2$  with expected value 1. (For a large number of degrees of freedom  $\nu$ , the distribution of  $\chi^2$  is approximately normal with mean  $\nu$  and standard deviation  $\sqrt{2\nu}$ .)

In the process of model fitting, a number *m* of parameters of the model are estimated from the data. This reduces the number of degrees of freedom from *M* to M - m, so the amplitude agreement factor, as defined above, is not strictly a reduced  $\chi^2$ . For Gaussian model fitting, *m* is usually small compared with *M*, so this distinction can be ignored, but for a clean-component model with hundreds of parameters (component flux densities and positions), *m* may be large, and the expected value of the agreement factor may be significantly less than 1.

When the data are self-calibrated, additional parameters (unknown antenna gains) are estimated from the data, so the number of degrees of freedom is reduced. For example, if the data are taken on an array of N antennas and N(N-1)/2 baselines and if independent gains are estimated for each antenna for each integration, the number of degrees of freedom is reduced by a factor (N-3)/(N-1), and the expected value of  $Q_{AMP}$  is  $\sqrt{(N-3)/(N-1)}$  (e.g., 0.58 for N = 4 and 0.88 for N = 10). Wieringa (1992) has shown that for self-calibration with a perfect model, the noise in the visibility amplitudes after application of (noisy) gain solutions is *lower* than the noise in the input visibilities by a factor  $\approx \sqrt{(N-3)/(N-1)}$ . This leads to the reduction in the expected value of  $Q_{AMP}$  shown above. 1995ApJS..100...1H

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## A2. CLOSURE-PHASE AGREEMENT FACTOR

Closure phase is the sum of visibility phases around a triangle of baselines; e.g., for three antennas i, j, k,

$$\psi_0^{(ijk)} = \phi_0^{(ij)} + \phi_0^{(jk)} - \phi_0^{(ik)}.$$
(2)

In the high-SNR approximation, the variance of the closure phase is given by

$$(\sigma_{\psi}^{(ijk)})^2 = (\sigma_{\phi}^{(ij)})^2 + (\sigma_{\phi}^{(jk)})^2 + (\sigma_{\phi}^{(ik)})^2.$$
(3)

In an array of N antennas in which all baselines are measured, there are N(N-1)/2 visibility phase measurements from which N(N-1)(N-2)/6 closure phases can be formed. However, only (N-1)(N-2)/2 of these are independent.

The closure-phase agreement factor is defined in a similar way to the amplitude agreement factor but allows for the fact that the closure phases are not all independent:

$$Q_{\rm CLP} = \sqrt{\sum_{1}^{M_{\rm CLP}} f\left(\frac{\psi_0 - \psi_m}{\sigma_\psi}\right)} / \sum_{1}^{M_{\rm CLP}} f , \qquad (4)$$

where the sum is taken over all  $M_{CLP}$  available closure-phase samples, but the denominator  $\sum f$  is now the number of independent closure phases, and the factor f is computed for each sampling interval as the number of independent closure phases divided by the total number of closure phases in that interval. If all baselines were observed, then f = 3/N.

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