DEEP CCD PHOTOMETRY AND VARIABLE STARS IN THE METAL-RICH GLOBULAR CLUSTER M71

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ABSTRACT

Two sets of observations of the metal-rich globular cluster M71 are presented. The first uses deep CCD exposures to derive a fiducial in V, B - V and compares this with a cluster of similar metallicity, 47 Tuc. Comparison with oxygen enhanced theoretical isochrones leads to age estimates for M71 of from $\sim 14 \pm 2$ Gyr to $\sim 16 \pm 2$ Gyr. Within the limits imposed by the quality of the data, no significant age difference between the two clusters is found. The second set of 73 frames is used to search an overlapping 67" × 104" area of the cluster for variable stars. Light curves and phase diagrams (where appropriate) are presented for all four of the variables discovered. One variable blue straggler (or SX Phe star) has been identified with a period of 04050. Values for its mass depend, of course, on the assumed pulsation mode— $(0.90 \pm 0.47) \mathscr{M}_{\odot}$ for the first overtone mode, and $(1.57 \pm 0.83) \mathscr{M}_{\odot}$ for the fundamental mode. One of the variables, with a 040582 period, but with a magnitude 1 m75 below the main sequence turnoff may be a field star. Two candidate eclipsing binary systems were also found. The most likely orbital period of one is 04372. This value, and the shape of the light curve, suggest that it could be a W UMa type variable. No period was obtainable for the other candidate binary due to a lack of phase coverage. Further data is needed to confirm and strengthen these claims, and to check for cluster membership.

1. INTRODUCTION

The globular cluster M71 is a small, metal-rich cluster lying close to the galactic plane. Together with 47 Tuc it is one of the brightest and nearest of the "disk" globular clusters and can be studied in some detail. The first major modern work on M71 is that of Arp & Hartwick (1971), conducted using photoelectric and photographic observations. They noted the existence of a small number (≤ 10) of blue stragglers, and derived estimates for the age, reddening, metallicity, and distance. Cudworth (1985) gives photographic photometry and membership probabilities for stars in the M71 field brighter than $V \approx 16.8$. Richer & Fahlman (1988) identified both a sequence of white dwarf candidates and over 50 blue stragglers using deep CCD photometry of a large $(6' \times 4')$ area of M71. They also derived better estimates of the foreground reddening and distance modulus. A further study (Richer & Fahlman 1989) investigated both the mass and luminosity functions of M71 using the same data. Part of the previously unpublished data gathered for that work is presented here. Heasley & Christian (1991) compare their CCD photometry to the Hesser et al. (1987) photometry of 47 Tuc and claim an age difference of ~ 3 Gyr, with M71 being the older cluster.

Zinn (1985) presents convincing evidence for the existence of two populations of globular clusters (halo and intermediate), partly on the examination of the distribution of metallicity. Clusters with an [Fe/H] more metal rich than -0.8 can be identified with this latter population and M71 falls into this category. In support of this Allen & Martos (1988) show, by performing numerical integrations of the cluster's orbit backwards in time, that M71 has a very similar galactic orbit to the open cluster M67. In fact, in plots of metal abundance versus apocentric distance, pericentric distance and orbital eccentricity, M71 always groups with the galactic clusters in their sample rather than with the other globular clusters which tends to strengthen the idea that M71 is a disk population object. However it should be borne in mind that Allen and Martos use the cluster proper motions derived by Cudworth (1985), and that these are uncertain at almost the 50% level.

Sawyer Hogg (1973) catalogues four variable stars in M71, including an eclipsing binary. However Liller & Tokarz (1981) show, on the basis of its radial velocity, that the latter object is probably a field star. Cudworth (1985) notes that two other variables may also be present using data from that study in addition to a study by Welty (private communication to Cudworth) and one by Frogel *et al.* (1979) who cite Sawyer Hogg (private communication to Frogel *et al.*). All these variables lie near the tip of the red giant branch, and none are within the field studied in this survey.

The initial objective of this study, the preliminary results of which have been discussed in Hodder *et al.* (1991), was to search for variable blue stragglers in M71. However, the method employed in the data analysis enabled any type of variable with a period from approximately 30 min to 7 hr to be searched. Section 2 outlines the observations and calibration and Sec. 3 discusses the data analysis procedures. Section 4 presents a deep color-magnitude diagram for M71. Section 5 discusses the variables discovered, while Sec. 6 summarizes the results obtained in this study.

2. OBSERVATIONS AND DATA REDUCTION

2.1 The Deep Data

Richer & Fahlman (1988) presented a search for white dwarfs in M71 using deep CCD photometry of the inner $6' \times 4'$ of the cluster. This was accomplished using U, U - Vphotometry—the *B* data was not presented. Here we present the *V*, B - V photometry of the NE field described in the Richer and Fahlman study. In addition to the deep photom-

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etry we have included the results from short exposure frames to study the giants and horizontal branch stars.

A more complete description of the data is given in Richer & Fahlman (1988)-a brief summary is given here. The observations were made on 1986 August 2/3 using the double density RCA CCD detector at the prime focus of the 3.6 m Canada-France-Hawaii Telescope. The full width at half maximum (FWHM) of the point spread functions of these frames is typically 0"7, and no frame with a FWHM greater than $0^{\prime\prime}$ 8 was used in the reductions. The deep V exposure times were 600 s long and the best three frames were averaged together to produce a final frame. The deep B exposures were 900 s long and the best two were averaged. Two short (60 s) exposure frames, one each in V and B, were obtained to study the giant branch. During the whole observing run a total of four fields were observed-the northeast field generally had the best image quality and the photometry from it is presented here. The long exposure and short exposure data were calibrated independently. Standard colors (B - V), were obtained from the instrumental colors (b - v), through an equation of the form

 $(B - V) = \alpha(b - v) + \text{constant.}$

The color coefficient, determined from equatorial standards, was found to be 1.27, consistent with other photometry done with this chip and filter combination at CFHT. No color term was needed for the V transformation. An unexplained systematic offset was found between the long and short exposure datasets. These mean offsets (calculated from 520 stars) were

$$B_{\text{long}} - B_{\text{short}} = 0.090 \pm 0.064,$$

 $V_{\text{long}} - V_{\text{short}} = 0.119 \pm 0.068.$

The short exposure frames were of noticeably poorer image quality and seeing than the long exposure frames. Consequently magnitudes derived from the short exposure frames had higher photometric errors and were therefore shifted onto the long exposure system. This data set was then used to calibrate the data for the variable star search.

2.2 The Variable Search Data

The CCD frames used in the search for variable stars were taken during the nights 1985 July 11/12 to 14/15 at the 3.6 m Canada–France–Hawaii Telescope by H.B.R. and G.G.F. The RCA1 chip was used at the f/8 Cassegrain focus resulting in a plate scale of 0"21 per pixel. A total of 87 frames of approximately the same field of M71 were taken over that period, of which 75 were reduced for this analysis. The remaining 13 were not reduced owing to the poor seeing, and consequently increased crowding, on those images. A log of the observations is given in Table 1. Approximately the same

TABLE 1. Condensed observing log.

Date	Time (U.T.)	V frames	B frames	Field
(1)	(2)	(3)	(4)	(5)
1985 July 12/13	08:34 - 14:37	23	9	Variable search
1985 July 13/14	08:24 - 14:08	2	11	Variable search
1985 July 14/15	05:43 - 14:56	0	2	Variable search
1985 July 15/16	10:11 - 13:58	15	9	Variable search
1986 August 2/3	11:35 - 12:54	3L/1Sª	2L/1S ⁶	Large field exposures

a) Long exposures (L) were 600 s; short exposure (S) 60 s

b) Long exposures were 900 s; short exposure 60 s

area (67" \times 104"), centered 30" north and 55" east of the cluster center was observed in each case. This field is almost completely contained in the NE field of the deep photometry. The seeing in the V band on each of the four nights was typically 0".7, 1".0, 0".6, and 0".5, respectively.

After preprocessing each frame was reduced using the DAOPHOT computer program (Stetson 1987) to produce lists of coordinates and magnitudes for each star on the frame. The number of stars measured on each frame ranged from ~ 1800 on the best frame to ~ 700 on the worst frame. A list of 20 moderately bright (but unsaturated) and uncrowded stars was compiled to determine the PSF for each frame. Because of variations in seeing and position of each frame, typically a dozen stars from this list were finally used in the determination of each PSF. Positions and magnitudes for each star on the frame were determined by the DAOPHOT profile fitting software packages described in Stetson (1987).

Calibration of the 1985 time series data was achieved using a two step process. First, stars from the calibrated long exposure frames of 1986 were identified in two 1985 reference frames, one in each filter. Stars with an error in B and Vin the long exposure frames of more than 0m02 were excluded, leaving 56 stars for the calibration of the reference frame. Then the offsets between the calibrated reference frame and the other frames in the time series were determined as follows. A list of stars found on all time series frames was compiled. For each of these frames the mean magnitude difference between it and the reference frame was calculated using the stars on this list. The mean difference for a given frame was then applied to all the measured magnitudes on the appropriate frame thus placing it on the same magnitude scale as the reference frame. The standard deviation of these mean magnitude differences were of the order of 0^m001 to 0^m0001. These errors were added in quadrature to the appropriate magnitudes.

3. A DEEP COLOR-MAGNITUDE DIAGRAM

3.1 Photometry

The photometry from both the long and the short exposure frames obtained in 1986 was combined to produce a color-magnitude diagram (CMD) as follows. The final lists of photometry were matched together and compared. If a star appeared on both lists and its V magnitude was brighter than 17.5, the data from the short exposure frames were used, otherwise the data from the long exposure frames were used. The color-magnitude diagram resulting from the final data list is tabulated in Table 2. An attempt was then made to identify stars brighter than V = 16.85 with stars from Cudworth's (1985) study. Of the 116 such stars, 77 were identified with a Cudworth star. Of those 42 had a cluster membership probability of 50% or more and are marked with a * in Table 2. The variable stars discussed below are indicated in this table by a number in parentheses to the left of the star number in column (1).

Figure 1 is the color-magnitude diagram of the data in Table 2. In order to reduce the scatter around the giant branch above V = 16.85 (Cudworth's magnitude limit) we have only plotted those stars with a 50% (or greater) chance of being cluster members. Below this limit all stars are plotted. Also shown in Fig. 1 is a line marking the position of the horizontal branch at $V_{\rm HB} = 14.44 \pm 0.08$ (the mean V magnitude of the 12 stars in that region of the CMD). From Arp

e	×	≻	A	B - V	U - B	A	×	≻	2	B - V	U - B	B	×	≻	2	B = V	U - B
- °	501.3 146.6	647.8 62.9	12.18	1.17	1.85	60	372.	339.0	0 16.02 16.08	1.15	1.21	131	122.	1720	16.98 16.98	1.16	-0.12
÷.	77.0	456.7	12.35	1.60	1.79	. 89	107.	3 256.5	16.08	1.15	0.50	133	402	0.41 L	16 98	201	0.53
*	194.8	670.2	12.46	1.72	1.26	69	471.	649.3	16.09	1.23	1.25	134	211	5 712.7	16.98	0.76	0.25
\$°	472.6	385.5	12.46	1.58	1.95	04 *	31.	222.6	16.09	0.72	-0.17	135	14.	3 775.7	17.03	1.25	0.33
٩ :	148.0	162.1	12.42	1.56	2.01	7.6	340.	275.5	16.11	9.1	0.51	136	165.	57.8 57.8	17.03	1.01	0.23
• •	152.9	484.5	12.52	1.67	1.91	. 5	52.0	15.0	16.13	1.69	1.23	138	626	1 442.7	17.05	107	0.58
6 *	162.7	46.7	13.11	1.48	1.40	74	529.	1 766.3	16.18	0.64	0.15	139	158.	7 34.9	17.06	0.97	0.08
•10 •	593.7	177.3	13.24	1.26	1.27	75	221.	121.3	16.20	1.03	0.55	140	228.0	5 431.0	17.09	0.90	0.44
F;	106.0	-2.7	13.40	1.51	1.1	22 27	383.	401.0	16.21	1.00	0.47	141	451.	1 193.2	11.11	0.96	0.40
13 13	410.5	33.9	13.58	1.28	0.95	78	177.0	359.4	16.24	1.06	-0.03	143	541.	162.0	11.71	60 T	14.0
; 1	375.6	800.5	13.59	1.23	1.31	64	115.1	254.6	16.25	1.13	0.49	144	604	0.401 1	17.13	1.19	1.10
*15	132.4	179.0	13.67	1.33	1.17	80	399.0	188.1	16.25	0.77	0.31	145	215.	187.5	17.13	0.98	0.41
*16	226.4	111.3	14.25	1.21	1.01	(1) 81	454.(137.6	16.25	0.57	-0.21	146	377.	18.1	17.14	0.58	0.79
*17	269.5	71.8	14.32	1.01	0.51	82	186.0	312.5	16.25	0.86	0.19	147	489.0	369.4	17.15	0.96	0.44
*18 *18	625.6	210.6	14.33	1.05	0.63	*83	264.0	735.6	16.28	0.92	0.49	148	353.9	29.1	17.17	1.03	0.30
6T.	136.1	280.2	14.37	00'T	0.20	10 10 10	276.0	237.3	16.01	1.02	0.07	149	27.	1 190.9	17.17	1.11	0.51
*21	595.0	380.3	14.37	1.19	0.98	98	75.	14.4	16.32	1.18	0.51	151	577.	1 323.9	17.27	0.99	0.51
*22	190.8	274.7	14.38	1.06	0.47	87	618.9	219.1	. 16.32	1.03	0.85	152	556.	1 779.6	17.28	0.90	0.33
*23	278.5	93.7	14.40	1.04	0.52	88	566.	522.0	16.40	1.22	0.85	153	66	1 48.3	17.29	0.89	-0.23
а 1 2 4 2 4 3 4 4 3 4 4 3 4 4 3 4 4 3 4 4 3 4 8 4 8	157.2	695.7 737 K	14.43	1.27	1.38	50	181	245.1	16.42	0.97	0.29	154	320.1	503.4 70.5	17.29	0.76	-0.05
59 70	152.2	493.7	14.45	101	0.51	26 16	149.0	395.6	16.47	1.03	0.47	156	230.2	82.1	12 21	5 C	
27	404.5	657.5	14.47	1.34	1.51	92	511.	860.3	16.52	1.20	0.89	157	213.1	82.7	17.32	0.90	0.02
*28	138.4	265.7	14.48	1.10	0.39	93	22.	393.6	16.52	1.52	1.31	158	485.	5 193.2	17.32	1.10	0.82
*29	447.9	668.0	14.51	0.91	0.52	2	107.	10.4	16.52	1.25	0.35	159	253.0	761.8	17.33	0.94	0.43
*30 *	512.3	45.4	14.52	1.12	0.81	36	195.0	748.1	16.53	0.97	0.36	160	63.	7 163.3	17.33	0.75	0.59
IE.	626.1 262 r	560.0	14.52	1.07	0.50	88	168.	180.7	16.60	1.05	0.45	191	278.	5 756.3	17.35	0.65	0.15
*33	1.811	100.0 617.2	14 55	06.0	0.52	6	525	6573	10.01	0.90	0.50	162	153.0	117.0	17.35	0.81	-0.12
346	244.3	772.6	14.82	1.33	1.48	8	515.1	150.6	16.63	1.00	0.50	164	453.0	117.7	17.36	8.1	1.05
*35	279.0	114.4	14.83	1.15	0.80	100	221.4	373.5	16.64	0.96	0.47	165	478.	836.0	17.36	0.68	-0.09
36	45.4	233.8	14.93	1.26	0.67	101	200.6	112.7	16.64	0.97	0.37	166	320.1	5 239.7	17.37	0.76	0.32
*37	239.9	623.0	14.94	1.09	0.73	*102	373.9	225.4	16.64	0.87	0.28	167	192.8	3 224.3	17.39	0.96	0.26
8 <u>8</u>	103.7	377.1 178.6	15.01	21.1	0.78	101	213.1	708.0	16.68	0.98	0.48	168	216.4	434.7	17.40	0.91	0.38
\$ \$	363.6	661.8	15.10	101	0.71	105	16.4	340.5	16.69	0.77	-0.12	170	511.4	8.6	17.41	10.1	0.26
41	54.5	235.6	15.16	1.25	0.55	106	189.1	164.8	16.69	0.63	-0.06	171	401	175.2	17.41	0.82	0.16
*42	139.8	236.8	15.22	1.18	0.62	107	633.0	514.3	16.70	0.66	-0.07	172	536.4	E 34.5	17.42	0.72	-0.04
44	207.0	727.7	15.25	0.83	0.34	108	120.1	102 4	16.72	0.86	-0.21	173	288.	280.9	17.43	0.83	0.44
***	108.9	168.0	15.36	1.19	0.63	110	84.5	221.6	16.75	1.10	0.43	175	180.0	462.0	17.44	28.0	0.39
46	375.4	521.4	15.36	1.49	1.55	111	45.7	28.5	16.76	1.05	0.24	176	478.9	894.8	17.44	0.81	0.0
4	84.8	720.2	15.40	0.78	0.01	112	145.3	74.3	16.77	1.34	0.47	177	76.3	247.6	17.45	0.91	0.02
9 9	040.9 180.0	426.0	15.40	1.30	1.37	114	0.202	1.120	16.82 16.82	1.02	0.43	178	189.9	464.1	17.46	0.81	0.08 8 5
202	301.1	34.0	15.42	1.39	1.23	115	76.97	52.9	16.84	1.14	0.20	180	532.3	359.1	17.48	66°0	0.36
51	218.7	141.6	15.47	0.70	0.10	116	89.7	381.0	16.86	1.10	0.48	181	49.5	20.5	17.48	0.97	0.16
• • •	109.2	91.4	15.48	1.13	0.21	117	498.3	155.1	16.91	0.93	0.56	182	524.6	418.6	17.49	0.92	0.29
201	0.000	307.0	15.50 1 K KO	9 8 1	50.0 9 8 0	110	2111	645.7	16.01	1.92	0.16	183	354.2	242.0	17.49	0.81	0.31
22	102.0	529.9	15.59	1.12	0.60	120	421.4	699.2	16.92	0.65	0.22	185	360.0	8-96-6	17.50	0.82	0.11
*56	324.3	458.8	15.67	1.07	0.63	121	593.7	116.4	16.93	0.00	0.28	186	139.0	503.1	17.51	0.95	0.05
57	57.5	601.1	15.69	1.12	0.60	122	569.5	94.1	16.93	0.90	0.23	187	247.2	247.1	17.51	0.85	0.20
	310.7	384.5	15.77	0.97	0.52	123	254.5	321.1	16.94	0.99	0.40	188	273.8	631.9	17.52	0.90	0.19
	1.10.5	0.62	15.77	1.17	0.52	125	122.4	837.9	16.96	0.85	0.13	190	2555.2	306.0	17.52	0.87	0.26
61	14.5	498.7	15.81	1.19	0.49	126	145.0	28.9	16.96	1.24	0.38	191	196.9	190.3	17.52	0.94	0.26
62	530.0	286.7	15.89	0.89	0.44	127	48.4	216.5	16.96	0.99	0.76	192	511.6	213.1	17.52	0.88	0.19
83	е7. к	886.4 360.2	15.96	1.35	1.46	128	30.3	74.3	16.97	0.90	-0.13	193	461.8	159.1	17.53	0.91	0.28
5 8	40.4	820.3	16.00	1.09	0.58	130	310.9	53.0	16.98	0.87	0.02	195	514.0	373.9	17.53	0.84	0.10

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101	479.1	372.5	17.53	0.62	*T.0	192	1040		0.0	7.66	10.0	0.03	7020	401		1 11.19 2 17.80	1 23	0.00
108	42.2	1.02 202	17 54	0.74	0.00 44 0	707 797	921			7.67	0.88	60.0	328	496	7 328	1 17.80	1.22	0.85
061	349.1	158.7	17.54	180	14	264	108		122	7.67	0.81	0.14	329	350	0 346	2 17.80	0.76	0.00
200	233.9	809.7	17.56	0.88	0.22	265		•	1.6	7.67	0.82	0.16	330	369	0 117.	8 17.81	0.80	0.06
201	298.2	67.9	17.56	0.89	0.25	266	3 219	.6 1!	9.4 1	7.67	0.81	0.04	331	348	7 109.	7 17.81	0.78	0.07
202	120.3	781.5	17.56	0.81	0.28	267	304	5	8.0	7.67	0.72	0.19	332	236	0 860.	6 17.81	0.81	0.03
203	176.6 38.6	221.5	17.57	0.66	-0.02	268	123	0 4 0 4	5.0 7 7	7.67	0.75	90.0	(4) 333 334	91 8 10	307	8 17.81 8 17.82	0.49	-0.33
205	23.1	4	17.57	0.73	0.03	270	22	1 9	7.5	7.68	0.81	0.13	335	233	2 519.	1 17.82	0.82	0.10
206	424.2	822.2	17.57	0.92	0.35	271	601	8	5.9.3	7.68	0.79	0.04	336	i 436	.3 355.	5 17.82	1.00	0.70
207	188.0	353.2	17.57	0.67	-0.03	272	233	5 E	3.4 1	7.68	0.78	0.07	337	167	0 267.	8 17.82	0.79	0.05
208	304.5	214.7	17.58	0.87	0.25	273	5	20 i 20 i	6.63	7.68	0.81	0.11	338	3 226	.9 45.	0 17.82	0.74	0.08
209	70.6	543.8	17.58	0.87	0.18	274	356		0.0	7.68	0.73	0.26	339	• 1 68	8 260. 5 250.	5 17.83 K 17.93	0.79	0.05
511	530 G	1/2.0	17 58	0.00	0.23	926			, 1 1 1 1 1 1 1 1	7.69	0.80	0.02	341		4	2 17.83	0.79	0.28
212	414.6	781.0	17.58	0.84	0.52	277	232	30	8.2	7.69	1.25	1.19	342	144	0 29.	8 17.83	0.05	0.42
213	607.6	81.7	17.59	0.81	0.10	278	543	8.	17.8	17.69	0.79	0.08	343	69	3 251.	8 17.83	0.80	0.06
214	264.2	83.6	17.59	0.78	0.08	379	505	.4 2!	8.8	7.69	0.79	0.03	344	1118	7 448.	4 17.83	0.80	0.05
215	150.7	417.3	17.59	0.91	0.13	280	633	2 E	8.9	7.69	0.81	0.06	345	140		6 17.84	0.77	0.12
017	4.002	603.9	69'.1	1.01	\$T.0	107			0 1	0.1	70.0	0.00	040	107	2 I J C	10.11 ±	5.0	11.0
218	1.10	218.0	17 69	0.55	0.09 87 0	282	323			171	0.93	0.27	348	456	6 225	2 17.84	0.77	0.00
219	272.1	588.5	17.60	0.94	0.35	284	126			7.71	0.84	0.02	349	126	8 381.	7 17.85	0.70	0.09
220	235.6	208.5	17.60	0.67	-0.07	285	529	19	20.7	17.71	0.80	0.05	350	316	6 418.	6 17.85	0.78	0.07
221	355.0	455.1	17.60	0.82	0.17	286	314	.6 3	11.6 1	17.71	0.77	0.03	351	112	5 683.	5 17.85	0.81	0.12
222	568.9	324.2	17.60	0.92	0.22	287	366	.2 76	36.4 1	7.72	0.77	0.04	352	59	6 77	4 17.85	0.75	0.09
223	618.8	117.5	17.60	0.78	0.07	286	294	4	6.2	7.72	0.79	0.04	353	132	1 85.	7 17.85	0.77	0.05
224	378.2	652.6	17.60	0.88	0.16	285	43	è.	17.4	7.72	0.78	0.25	354	1256	2 100	9 17.86	0.84	0.14
225	473.2	83.5	17.60	0.75	90.08 0.08	290				1.72	0.95	60.0-	305		200	08.71 U	0.75	0.13
226	71.2	192.6 60.6	17.60	0.82	0.14 0.10	162		20 C	0.0	7 73	0.81	60.0	350 2 8 2	013	280.	2 I7.85	0.76	9.0 6
228	120.7	36.7	19.71	18.0	0.15	293	325	9 6 9 6	6.0	7.73	0.73	0.20	358	136	7 224	9 17.87	0.81	0.12
229	48.7	254.4	17.61	0.89	0.22	294	322	2	1.8	7.73	0.80	0.33	359	567	4 87.	0 17.87	0.83	0.08
230	229.6	553.3	17.61	0.89	0.24	295	91	.3	19.8	7.73	0.81	0.19	360	236	0 328.	1 17.88	0.78	0.03
231	76.1	248.2	17.61	0.73	0.43	396	3 154	89.	0.5	7.74	0.76	0.07	361	317	0 139.	8 17.88	0.80	0.06
232	34.1	330.2	17.61	0.76	0.12	297	49	· 5	9.8	7.74	0.80	0.03	362	302	2 678.	8 17.88	0.79	0.02
233	472.1	688.4	17.61	0.80	0.05	296			0.71	1.74	0.88	-0.02	363	193	6 137.	2 17.88	0.81	0.04
23 4	512.7 575 2	82.5 101	17.61	1.0.0	-0.03	008	104	5.0		174	2.0 0.90	-0.04	207 798	472	0 253	0 1/.00 6 17.88	60'D	0.00
236	287.8	355.1	17.62	0.83	0.25	301	154	, 0 , 0	6.11	7.75	0.73	0.21	366	583	6 432.	4 17.89	0.78	0.06
237	74.4	152.6	17.62	0.84	0.23	302	523	.3	1.5	7.75	0.80	0.08	367	20	6 13.	2 17.89	0.88	-0.01
238	100.4	75.2	17.62	0.70	0.12	303	499	.1 56	50.6	7.75	0.76	0.12	368	515	0 142.	0 17.89	0.81	0.05
239	175.9	319.1	17.62	0.81	0.12	304	••••••••••••••••••••••••••••••••••••••	- -	6.0	7.75	0.99	0.09	369	422	5 860. 241	6 17.89	0.80	-0.02
241	136.6	503.5 002 e	70'JT	0.80	20.0	305	1 1 2 4 C 7			7.76	61-0 24 0	0.05	370	507	5 120	5 17.89	0.70	0.03
242	250.3	142.0	17.63	0.82	0.08	307	557	4		7.76	0.79	0.07	372	186	2 193.	2 17.89	0.78	0.02
243	206.0	40.1	17.63	0.87	0.19	308	167	.1 26	57.7 1	7.76	0.88	-0.09	373	1 203	3 198.	4 17.89	0.74	0.12
244	281.9	174.6	17.63	0.86	0.12	308	40	е,	7.7	7.76	0.79	0.08	374	248	9 147.	5 17.90	0.80	0.01
245	177.4	11.2	17.63	0.89	0.27	310	122		9.9	7.77	0.81	0.04	375	514	2 165.	17.90	0.74	0.07
247	343.0	339.0 605 2	10.11		0.00	311	202	4 2 4 4	0.0	777	61.0	0.10	275	160	150	06.11 0	0.19	
248	108.3	587.1	17.64	0.86	0.05	. 313	133		1.6	7.77	0.79	0.12	378	394	3 580.	1 17.90	0.86	0.28
249	257.6	523.0	17.64	0.84	0.22	314	608	.3 71	8.2	7.77	0.71	0.11	379	169.	6 159.	5 17.90	0.78	-0.00
250	139.1	670.0	17.65	0.83	0.06	315	260	000	11	7.78	0.85	-0.09	380	113	9 349.	6 17.91	0.64	0.10
251	25.3	42.8	17.65	0.88	11.0	310	201	0.0	 	7 70	02.0	07.0		470	212 2	16'/1 4	67.0	20.0
253	164.4	200.9 94.7	17.65	0.85	20.0	318	415	9 0 9 0	3.4	7.79	0.78	0.04	383	193	8 137.0	16.71 0	0.78	0.10
254	36.3	61.9	17.65	0.83	0.08	319	251	.2	3.3	7.79	0.82	60.0	384	173	2 201.	9 17.92	0.79	0.02
255	390.4	306.1	17.65	0.77	0.07	320	50	4	3.6	7.79	0.76	0.02	385	492.	4 188.	4 17.92	0.78	0.05
256	350.5	45.7	17.65	0.77	0.22	321	302	ю. 2	1.7.1	7.79	0.75	60.0	386	394	4 580.	1 17.92	0.89	0.25
258	72.5	833.1	17.66	0.86	0.23	323	364	180 190	20.0	2.79	0.81	-0.03	388	378	0 376.4	8 17.93	0.79	0.01
259	557.9	316.0	17.66	0.82	0.11	324	363	5	1 6.3	7.79	0.79	0.15	389	459.	8 270.1	5 17.93	0.77	0.04
260	472.3	557.3	17.66	0.79	0.15	325	225	o.	3.3 1	7.79	0.75	0.07	390	572.	7 170.0	6 17.93	0.77	0.01

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	•		-					TABLE	2. (conti	nued)							
A	×	×	2	B - V	U - B	8	×	۲	2	B - V	U - B	A	×	7	Δ	B - V	U - B
391	495.4	350.0	17.94	0.81	0.04	456	245.2	38.8	18.09	0.80	0.0	521	120.	0 147.2	18.21	0.81	0.13
393	412.7	590.6	12.94	0.81	0.0	458	363.0	229.9	18.09	0.77	0.03	523	527	5 211.3	18.22	0.78	0.03
394	66.0	745.8	17.94	0.83	0.09	459	347.8	273.4	18.09	0.83	0.02	524	332	5 548.1	18.22	0.79	0.12
395	382.5	378.1	17.94	0.79	0.05	460	375.3	431.4	18.09	0.71	0.11	525	225.	.2 797.7	18.23	0.79	0.03
396	390.0	14.5	17.95	0.78	0.07	461	507.0	289.2	18.10	0.88	0.41	526	213.	.6 11 4 .6	18.23	0.88	0.07
395	1131	217.9	17.95 17.06	0.76	-0.01	462	507.1	289.0	18.10	0.78	# 0 0	525	120	5 93.8 8 112 1	18.23	0.70	0.77
399	1.011	492.9	17.95	0.85	-0.01	4 4 4	39.1	674.5	18.11	0.86	0.04	520	395.	7 729.5	18.23	0.75	-0.01
400	258.9	443.2	17.95	0.79	0.07	465	129.4	409.2	18.11	0.86	0.24	530	570	4 79.9	18.23	0.80	0.04
401	98.7	107.4	17.95	0.73	0.12	466	191.9	232.6	18.11	0.91	0.06	531	603	.1 625.0	18.23	0.89	0.10
402	136.6	418.4	17.95	0.79	0.07	467	500.3	169.9	18.11	0.78	0.08	532	193	0 526.8	18.23	0.83	0.12
403	181.2	340.5	17.95	0.76	0.05	468	79.6	597.9	18.11	0.79	0.05	533	155.	8 701.3	18.24	0.80	0.09
1 04	284.0	170.9	17.95	0.80	0.05	469	450.5	1.7.1	18.11	0.78	0.02	534	193	2 530.8	18.24	0.81	0.10
404 404	6.024	350.1	17.95	8.0	0.03	24	1.4	13.9	10.11	0.'0 22	0.09	100	0.0	8 424.3	18.24	0.91	0.47
	1.50	0.45	06. J T		10.0-	1		0.007	11.01	04.0	60.0			- 114-9 7 - 114-9	10.24	0.0	
40 4	1.007	276.6	96.11	0.04	0.01	7.7	21127 215 8	219.4	10.12	0.76	0.05	100	1631	1826	16.20	0.00	5.0
40 1	412.8	538.2	96.11	200	10.0	474	453.7	171.3	18.12	0.66	-0.02		424	1 470.0	18 25	0.76	14
410	357.5	56.5	17.96	0.76	110	475	17.4	419.1	18.12	0.88	-0.06	540	218	9 27.8	18.26	0.84	110
411	159.1	193.7	17.97	0.77	0.16	476	425.6	817.1	18.13	0.73	-0.02	541	ŝ	0 799.3	18.26	62.0	0.12
412	240.5	369.6	17.97	0.78	0.08	477	262.6	2.8	18.13	0.86	-0.10	542	454	2 19.1	18.26	0.80	0.04
413	591.6	16.3	17.98	0.75	0.01	478	90.2	91.1	18.13	0.67	-0.07	543	225.	7 952.1	18.26	1.05	0.50
414	450.4	106.7	17.98	0.77	0.05	479	408.0	623.4	18.14	0.79	0.05	544	173	9 65.6	18.26	0.73	0.09
415	256.1	101.1	17.98	0.65	0.11	480	438.1	100.7	18.14	0.71	-0.06	545	251.	2 53.8	18.27	0.78	0.04
416	309.1	448.7	17.98	0.79	0.05	481	192.4	402.5	18.14	0.78	0.03	546	424	8 356.5	18.27	0.77	0.03
417	117.4	48.6	17.98	0.77	0.04	482	399.0	670.8	18.14	0.89	0.40	547	124	5 97.6	18.27	0.79	0.03
418	117.5	194.1	17.98	0.79	0.04	483	27.1	57.5	18.14	0.71	0.20	546	228	.2 417.5	18.27	0.80	0.08
419	310.0	432.2	17.98	1.17	1.08	484	160.4	27.7	18.14	0.77	0.21	546	49	8 400.5	18.27	0.79	0.12
420	183.2	41.5	17.98	0.78	0.10	485	516.3	279.5	18.14	0.80	0.02	550	199.	.1 383.8	18.27	0.79	0.06
421	631.5	117.9	17.98	0.77	0.06	486	161.4	332.4	18.15	0.77	0.07	551	245	4 104.2	18.28	0.79	0.07
422	216.8	47.3	17.99	0.78	0.03	487	451.0	545.4	18.15	0.84	-0.01	552	50	7 154.2	18.28	0.75	0.74
423	167.6	172.2	17.99	0.83	0.00	488	308.5	872.4	18.15	0.79	-0.04	553		.2 24.5	18.28	0.77	-0.04
424	280.1	935.0	17.99	0.82	0.00	489	98.2	391.0	18.15	0.80	0.17	554	80	.0 32.7	18.28	0.76	0.24
425	62.9	749.0	18.00	0.84	0.14	1 90	116.5	578.7	18.16	0.79	0.08	555	563.	4 391.1	18.28	0.83	0.28
426	333.6	592.2	18.00	0.79	0.08	491	98.1	204.4	18.16	0.84	0.08	556	8	0 155.3	18.28	0.75	0.04
427	375.7	431.5	18.00	0.75	0.03	492	21.3	13.7	18.16	0.60	60.0	221	213	4 114.8	18.28	0.74	0.10
428	503.2	84.3	18.01	0.79	0.17	1 93	319.4	329.4	18.16	2.0	50.0		19	9 81.3	18.28	0.75	0.15
624	53.7	357.1	18.01	0.76	0.11	16	140.2	315.8	91.91	82.0	20.0	200		2 36.3	18.28	1.10	-0.21
02 7	307.0	03.0	18.02	0.00		061	- 102 -	0.100	01.0T	* °2	07.0	100		019.6	10.29	0.87	22.0
121	0.150	261.0	10.01	2.4.0	20.0	104	1.000	206.2	11 17		500			0 001.5	10.49	70.0	91.0
18	56.5	637.5	18.02	60.0	0.38	108	264.5	497.7	18.17	0.84	0.13	563	167	5 652.8	18 30	0.00	
434	276.7		18.02	0.85	0.25	69	41.7	407.6	18.18	0.79	0.12	564	285	7 41.3	18.30	86.0	0.64
435	610.9	157.9	18.03	0.82	0.03	200	140.3	315.7	18.18	0.84	-0.05	565	212.	1 806.7	18.30	0.84	0.17
436	551.1	457.3	18.03	1.02	0.70	501	181.6	564.9	18.18	0.80	0.08	566	94	0 377.2	18.30	0.74	0.29
437	473.3	920.4	18.03	0.80	3.12	502	30.5	36.9	18.18	0.78	-0.03	567	8	8 18.2	18.30	0.73	0.08
438	213.0	358.6	18.04	0.79	60.0	503	170.1	262.7	18.18	0.82	0.12	568	14	3 591.9	18.30	0.97	0.57
439	437.6	532.3	18.05	0.77	0.08	204	52.1	932.2	18.18	0.82	0.20	263	17.	8 110.2	18.30	0.85	0.24
440	189.4	0.1	18.05	0.98	-0.19	505	451.0	545.6	18.18	0.78	0.05	570	44	1 531.9	18.30	0.85	0.32
1	203.0	1.187	10.05	69.0	15.0	8	340.2	230.0	10.10	220	0.00		010 1	1133.2 1133.2	16.31	0.78	0.0 10
142	2006	LU1.3	10.05	0 2 0 2	91.0		1.0.1	0.7.0 A C	18 10	0.75	17.0		1 / 0	1 113.2	16.31	0.80	0.02
1	252.5	5.2	18.06	0.00	80.0	89	164.0	236.6	18.19	16.0	0.36	574	317.	6 117.0	18.31	0.79	20.0
445	386.0	182.1	18.06	0.81	0.05	510	338.4	198.5	18.19	0.80	0.03	575	407.	8 496.4	18.31	0.78	0.08
446	119.9	81.4	18.06	0.81	0.10	511	288.2	74.5	18.19	0.82	0.05	576	372.	8 183.0	18.31	0.88	0.20
447	598.8	11.7	18.07	0.78	0.16	512	399.9	340.5	18.19	0.77	0.03	577	419.	9 328.5	18.31	0.76	0.04
448	115.3	110.2	18.07	0.70	0.13	513	126.8	217.0	18.19	0.88	0.12	578	290.	4 153.3	18.31	0.81	0.02
44 9	415.2	136.2	18.08	0.80	0.02	514	583.8	467.6	18.19	62.0	0.08	579	319.	254.2	18.32	0.78	0.14
420 4 1 1	533.2	535.2	18.08	0.81	-0.06	515	75.5 • •	861.3	18.20	1.23	1.17	58U 58U	5	7 297.5	18.32	0.78	0.08
452	452.7	432.6	18 08	5.0	27.0	212	112.1	389.1	18.20	0.76	0.10	582	389.	1 56.5	18.32	0.78	10.0 -
453	533.1	535.2	18.09	0.75	0.06	518	97.9	204.5	18.20	0.77	0.09	583	307.	8 207.2	18.32	0.81	0.03
454	258.5	188.5	18.09	0.80	0.02	519	12.0	126.3	18.21	0.70	0.08	584	322.	3 305.2	18.33	0.75	0.05
					100		1 010	0.00	10.01	0 2 3	0.16	KOK	136				

	U - B	0.04	0.39	0.08	0.10	0.32	0.49	0.11	0.06	-0.11	0.15	0.07	0.12	0.07	0.09	0.14	0.14	0.12	0.07	0.15	0.13	0.06	0.16	0.10	0.20	0.16	61-0	11.0		77.0		60°0	87.0	0.09	0.06	0.08	0.14	0.05	0.11	0.11	0.59	0.39	0.57	1.0	80.0 90.0	5.0	0.11	0.47	1.38	0.34	0.11	0.05	0.27	0.12	0.19	0.03	0.08	0.09	0.08	0.05	
-	B - V	0.87	0.64	0.80	0.01	0.89	0.75	0.80	0.80	0.90	0.73	0.84	0.74	0.82	0.81	0.81	0.84	0.82	0.81	0.83	0.41	0.84	0.86	0.83	0.83	0.81	62.0			70.0		10.0	0.00	0.83	0.63	0.83	0.87	0.82	1.02	0.84	0.23	0.90	0.91	1 6.0	0.62		0.84	1.13	1.40	0.78	0.86	0.83	0.97	0.79	06.0	0.74	0.85	0.83	0.84	0.81	000
	Δ	18.57	18.58	18.58	19.50	18.58	18.58	18.59	18.59	18.59	18.59	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.61	18.61	18.61	18.62	18.62	18.62	18.62	18.62	10.03	19 63	10.03	10.01	19.64	18.64	18.64	18.64	18.65	18.65	18.65	18.65	18.65	18.65	18.66	18.66	18.66	18.66	10.01	10.01	18.67	18.67	18.67	18.67	18.68	18.69	18.70	18.70	18.70	18.70	18.70	18.70	18.71	18.72	
	Y	223.9	103.9	74.0	1.50	34.1	343.6	718.4	690.2	223.6	25.2	423.3	149.7	249.4	323.9	459.4	95.4	599.5	33.5	477.1	103.4	1003.0	187.4	105.9	1.101	1 81.3	1.91	1.00	101.00	1.707	170.2	20.8	0.02	103.4	39.6	120.4	359.4	240.4	847.7	315.2	233.1	307.0	83.5	18.6	219.0	165.6	472.9	682.6	166.6	266.0	789.9	36.5	450.9	274.1	665.6	368.3	203.2	298.3	115.3	268.1	
	x	97.9	20.5	430.3	210.0	268.6	26.1	326.7	340.5	98.1	349.1	228.8	62.9	534.0	286.3	587.5	394.7	394.3	203.4	516.4	81.7	113.7	305.5	403.4	496.3	432.7	2.05	1007	14.9	0.600 6,0 0	010 0	0.714	615.6 515.6	448.7	459.9	242.9	480.2	525.1	397.7	594.7	190.6	289.4	517.4	176.1	1.002	2.020	478.2	185.4	618.7	548.3	135.3	220.5	190.2	12.7	100.2	160.6	24.0	557.4	551.5	787 5	
	A	716	112	718	617	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735	736	737	738	739	740	141	241		121	140 146	147	140	140	760	751	752	753	754	755	756	757	758	759	160	19,	201	764	765	766	767	768	769	770	111	772	773	774	775	776	444	
	- B	0.04	0.15	0.21	1.2.0	0.49	0.12	0.03	0.06	0.06	0.13	0.28	0.03	0.10	0.23	0.09	0.12	0.11	0.11	0.12	0.06	0.07	0.17	1.39	0.15	0.04	0.16		60.0	21.0	51.0	0.10	10.0	110	0.02	60'0	1.23	0.23	0.25	0.06	0.03	0.10	0.03	0.14	60.0	0.03	0.07	0.11	0.26	0.15	06.0	0.07	0.12	0.03	0.08	0.19	0.12	0.07	0.03	c1 c	AT-0
ued)	B - V U	0.85	0.81	0.88	0.95	0.96	0.89	0.80	0.80	0.81	0.80	0.74	0.81	0.77	0.83	0.78	0.82	0.78	0.80	0.79	0.91	0.84	0.76	1.53	0.88	0.83	0.79	50.T	19.0	5.0	10.0	0.00	0.02	82.0	140	0.82	0.89	0.85	0.99	0.82	0.79	0.80	0.80	0.83	0.84	6.0	0.81	0.77	06.0	0.82	0.91	0.79	0.82	0.75	0.82	0.84	0.81	0.78	0.80		0.78
contin	Δ.	18.46	18.46	18.46	18.46	18.47	18.47	18.47	18.47	18.48	18.48	18.48	18.48	18.48	18.49	18.49	18.49	18.49	18.49	18.49	18.50	18.50	18.51	18.51	18.51	18.51	18.51	10.01	18.52	16.52	70.01	10.52	10.04	18 52	18 53	18.53	18.53	18.53	18.53	18.53	18.53	18.53	18.54	18.54	18.54	10.54	18 55	18.55	18.55	18.55	18.55	18.56	18.56	18.56	18.56	18.57	18.57	18.57	18.57		18.57
TABLE (۲	200.7	303.7	33.2	20.6	0.020	155.8	110.1	399.1	616.2	555.0	136.2	315.4	237.1	422.4	45.8	453.0	283.5	386.5	181.3	37.0	640.0	6.3	331.3	442.9	139.4	250.4	2.200	408.6 408.6	29.1	7.01	10.01	1.120	125.9	23.0	119.8	491.4	73.5	390.2	959.2	54.5	630.0	246.4	610.0	769.0	9.109	1.000	398.6	767.1	560.8	598.1	288.5	638.7	809.2	143.0	544.6	429.3	176.4	223.8		216.6
	×	139.8	100.0	127.5	127.8	300.0	154.9	172.2	420.6	341.1	515.5	283.2	291.0	123.2	517.3	358.1	400.9	145.7	217.6	54.2	127.7	164.8	92.8	105.5	42.6	256.5	45.6	5.0.3	1.420	424.9	0.000	141.0	100.4	273.1	86.4	171.8	140.4	117.5	336.3	15.2	33.1	550.7	445.7	81.4	338.9	744.1	2.255.7	238.9	18.6	334.7	24.0	272.3	136.4	319.3	429.1	40.4	219.1	535.2	422.1		21.3
	A	651	652	653	65 4	000 686	657	658	629	660	661	662	663	664	665	999	667	668	699	670	671	672	673	674	675	676	677	8.0	6/9	080	190	790	200	185	990	687	688	689	690	691	692	693	694	695	696	169	009	200	101	202	203	704	705	106	707	708	709	710	111		211
	I - B	0.08	0.00	0.03	0.00	61.0	0.13	60.0	0.07	0.03	0.20	-0.01	0.04	0.02	0.04	0.01	0.07	0.63	0.07	0.23	0.05	0.11	0.07	0.10	0.39	0.02	0.10		970	28.0	0.00	0.15	50.0-	0.00	0.13	0.17	0.41	0.14	0.05	94	0.12	0.64	0.36	0.05	60.0	90-T	20.0	0.08	0.11	0.08	0.02	0.15	0.08	0.08	0.17	0.05	0.08	0.02	0.11	• • •	7T.0
	B-V (0.81	0.79	0.79	0.70	0.73	0.81	0.76	0.76	0.79	0.78	0.71	0.78	0.78	0.78	0.77	0.79	0.99	0.80	0.95	0.79	0.86	0.81	0.76	0.92	0.82	82.0		10.0	76.0	10.0	5.0		19.0	0.84	0.72	0.92	0.78	0.81	1.12	0.78	1.01	06.0	0.81	- 20 - 20	00-T	0.81	0.81	0.83	0.77	0.74	0.81	0.81	0.77	0.91	0.78	0.81	0.83	0.78		210
	Λ	18.33	18.33	18.33	10.33	18.34	18.34	18.35	18.35	18.35	18.35	18.35	18.35	18.36	18.36	18.36	18.36	18.36	18.37	18.37	18.38	18.38	18.38	18.38	18.38	18.38	18.38	10.09	10.39	10.39	60.01	10.39	18 40	18.40	18.40	18.40	18.40	18.40	18.40	18.40	18.41	18.41	18.42	18.42	18.42	10.43	18.43	18.43	18.43	18.43	18.44	18.44	18.44	18.44	18.44	18.44	18.45	18.45	18.45	10 45	01-01
	Y	78.6	116.9	385.9	30.Z	204.5	391.8	87.5	280.2	98.2	303.3	103.1	250.4	238.3	357.1	728.0	198.3	48.0	36.6	481.2	214.4	71.7	908.0	56.9	810.3	356.9	209.I	0.607	#-010	U. J.C.	164 0	0.20T	4 004	703.4	530.8	109.0	211.3	57.3	122.0	66.2	163.0	863.3	849.8	150.0	010.3	0.161	69.7	347.4	223.9	319.5	277.9	422.5	148.8	158.0	470.2	127.8	630.5	206.8	93.2	2124	0.101
	×	170.8	318.2	347.8	8.80 1 00	186.7	82.6	449.5	51.8	464.0	80.0	86.4	378.7	510.0	382.9	411.6	348.0	36.7	326.3	198.4	274.0	324.0	65.7	290.6	250.1	383.1	0.770	0.100	2.00	105.0	261 2	242 8	220.0	133.2	253.5	379.4	366.6	578.7	537.0	512.1	505.9	224.1	116.3	153.4	1.001	1.160	376.1	552.6	73.7	520.3	267.3	439.9	395.6	363.8	165.4	309.2	446.3	144.6	368.5	315	
	Ð	586	587	588	202	165	592	593	594	595	596	597	598	599	809	601	602	603	604	605	909	607	608	6 <u>9</u>	610	119	710	110	212	010 616	617	110	619	620	621	622	623	624	625	626	627	628	629	220	120	700 733	634	635	636	637	638	639	640	641	642	643	644	645	646	2.4.7	5

	U - B	0.12	0.22	0.15	0.13	0.17	0.13	0.30	0.26	0.33	0.17	12.0	0.20	0.34	0.45	0.12	1.16	0.14	0.18	0.13	0.16	0.15	0.13	0.16	0.14	0.12	0.19	0.44	0.18	0.49	0.46	0.22	0.26	0.30	0.25	0.14	0.78	0.83	0.20	0.28	0.20	0.15	0.23	0.47	0.84	0.21	0.50	-0.02	0.23	0.32	0.19	0.28	0.14
	B - V	0.60	0.84	0.89	0.87	0.86	0.86	0.72	0.93	0.77	0.89	0.80	1.03	0.88	0.56	0.80	1.19	0.83	0.77	0.84	0.83	0.87	0.87	0.76	0.80	0.77	0.85	0.88	0.90	0.96	0.96	0.84	0.79	0.52	0.85	0.85	0.63	1.10	0.83	0.91	0.86	0.86	0.88	0.99	0.71	1.03	0.95	0.62	0.85	0.85	0.90	0.88	0.87
	V	18.98	18.99	18.99	18.99	18.99	18.99	19.00	19.00	19.00	19.00	19.00	10.61	19.01	19.01	19.02	19.02	19.02	19.02	19.02	19.03	19.03	19.03	19.03	19.04	19.05	19.05	19.05	19.05	19.05	19.06	19.06	19.06	90.6T	19.06	19.06	19.07	19.08	19.08	19.08	19.08	19.08	19.08	19.08	19.08	19.09	19.10	19.10	19.10	19.10	11.61	11.61	11.01
	Y	751.3	318.7	23.0	873.7	202.6	289.5	350.4	100.2	392.6	151.1	20.4	278.5	587.2	366.0	777.6	587.6	257.3	14.5	497.0	317.3	161.7	338.3	14.7	113.4	29.7	152.6	532.0	493.2	97.6 887.3	855.8	122.4	109.2	220.6	586.3	350.2	92.0	159.4	294.2	211.3	265.6	263.7	249.8	438.7	42.2	577.4	80.3	247.4	366.7	299.5 413.8	218.4	44.5	60.9
	×	387.5	32.3	79.1	107.8	372.8	253.3	278.1	213.8	120.7	141.9	193.6	85.4	18.0	87.4	95.9 06.1	488.3	444.2	321.1	433.5 766.6	294.6	333.0	393.8	129.4	514.7	303.5 89.6	206.2	27.3	54.5	222.0	79.7	319.7	57.9	13.1	317.3	410.1	288.5	338.2	400.8	260.9	174.7	262.4	234.2	43.4	520.3	60.9 63.3	219.5	263.2	52.5	159.7	365.8	482.1	391.7
	Ð	911	913	914	915	917	918	919 920	921	922	923	924	926	927	928	929	931	932	933	93 4 036	936	937	938	626 040	940 041	942	943	944	945	946	948	949	950	951	953	954	955 056	957	958	959	96	30F3	8 963	964	965 200	966 067	- <u>8</u> 86	696	970	972	973	974	975
	– B	0.17	0.14	0.39	0.14	0.37	0.15	0.14	0.19	0.41	0.11	0.16	0.18	0.15	0.05	0.11	0.10	0.21	0.18	0.21	0.13	0.23	0.16	0.15	0.09	1.10	0.13	0.17	0.25	0.41	0.17	0.18	0.17	0.16	0.42	0.30	0.35	0.12	0.13	0.18	0.22	0.18	0.44	0.05	0.14	0.14	0.19	0.16	0.19	0.22 0.92	0.18	0.24	0.51
(p	-V U	0.82	0.84	F.06	0.82	.08	0.84	0.85	1.84	0.68	0.79	0.89	285	181	0.85	0.83	1.84	0.85	0.79	0.86 86	980	- 69.1	0.82	0.85	0.82	1.23	0.85	0.92	0.83	5.79	0.85	0.83	0.83	1.81	0.88	0.85	385	. 06.0	3.85	0.82	0.87	20.0	.87	0.34	0.86	0.85	1.79	0.87	0.88	0.83 0.6	201	.88	.98
ontinue	- B -	22	. E	5	99		5	55			8 8		9 g	5	6 6			5					20	8:	2:	22			8		: *	4	.	* 1	: *	*	5		20	5	<u>ب</u>	2 4	, o	-	5	55	;5	2	5	55		2	8
E 2. (C	V	5 18.6	18.6	5 18.8	2 18.8	18.5	3 18.5	18.8	8 18.6	1 18.5	7 18.8	18.5		8 18.8	2 18.5	18.0	18.9	8 18.9	3 18.9	9 18.0		8 18.9	1 18.9	3 18.5	18.1	18.9	8 18.5	5 18.9	1 18.5	18.0	4 18.5	4 18.9	8 18.9	18.5	18.9	9 18.9	18.5	8 18.0	1 18.9	8 18.9	9 18.9	201	18.6	4 18.9	9 18.5	10.5	18.5	18.5	1 18.9	8 18.9	2 18.9	18.9	1 18.5
IABL	Υ	322.1	913.5	29.1	394.1	475.0	359.3	132.5	184.1	261.	61	256.1	545.0	170.	772.		269.9	510.8	125.3	505.9	404	656.1	397.3	203.3	21.2	420. 17.1	45.8	89.	831.	372.1	572.	385.	57.8	457.	603	377.9	384.	216.5	274.	283.8	487.9	192	495.9	5	253.9	218.9	27.1	897.1	325.1	962.8	110.5	538.	963.1
	×	363.2	145.5	175.2	280.4	276.1	320.5	333.9 K2K 2	252.4	150.0	142.3	615.2	2.122	518.3	333.0	41.8	22.7	313.0	87.1	583.5	231.8	41.0	291.9	442.2	164.7	232.1	576.6	123.5	23.2	602.6	265.9	265.7	300.7	335.0	523.2	488.4	338.6	206.9	562.6	164.7	522.4	476.3 202 2	524.1	189.2	251.6	101.5	318.9	73.0	604.1	45.8 100 E	193.8	123.3	22.0
	Ð	846	848	849	850	852	853	854 855	856	857	858	859	86U 861	862	863	864	866 866	867	868	869	871	872	873	874	875 676	877	878	879	880	881	883	884	885	886 887	888	889	890	891 892	893	894	895	890 203	898	668	006	106	706 803	904	305	906 907	806	606	910
	U - B	0.43	0.19	0.10	0.14	0.22	0.38	0.03	0.06	0.14	0.19	0.16	01.0	0.09	0.17	0.11	0.23	0.08	0.19	0.06	6T-0	0.76	0.17	0.16	0.24	1.08	0.17	0.21	0.13	0.06	0.35	0.11	0.14	0.15	0.14	0.17	0.10	60.0	0.18	0.11	0.23	0.40	0.17	0.11	0.17	0.57	0.23	0.20	0.20	0.14	0.29	0.92	0.24
	B - V	1.10	0.80	0.79	0.82	0.83	0.88	0.88	0.87	0.78	0.83	0.82	0.03	0.83	0.77	0.71	0.92	0.84	0.86	0.82	0.00	1.05	0.87	0.81	0.84	1910	0.83	0.85	0.81	0.85	0.95	0.82	0.83	0.87	0.79	0.85	0.85	0.83	0.84	0.82	0.87	0.87	0.81	0.87	0.84	0.79	0.84	0.77	0.82	0.82	0.92 0.92	1.07	0.59
	V	18.72	18.72	18.73	18.73	18.73	18.73	18.73	18.74	18.74	18.74	18.74	18.74	18.74	18.74	18.74	18.75	18.75	18.76	18.76	18 76	18.77	18.77	18.77	18.78	18.78	18.78	18.79	18.79	18.79	18.79	18.80	18.80	18.80	18.81	18.81	18.81	18.82	18.82	18.82	18.82	10.02	18.83	18.83	18.83	18.83	18.83	18.84	18.84	18.84	18.85	18.85	18.85
	Y	74.7	220.2	330.9	96.1	517.1	842.5	189.1	1004.6	37.1	472.8	587.0	461.6 461.6	121.1	34.4	143.7	150.7	855.0	205.6	298.5	835.6	138.5	86.6	264.6	537.8	340.9 407.6	296.1	532.5	706.6	351.6	123.9	234.2	349.6	449.9 170 F	61.7	178.9	248.5	10.9 526.2	447.6	715.6	113.5	5.010 6.70.9	305.1	113.2	621.3	475.6	453.7	841.9	570.5	144.5	357.2	147.6	278.4
	x	134.2	500.6	437.7	595.8	300. r 184.5	108.6	630.2 101 F	118.4	346.4	326.3	454.4	1.000	570.7	425.9	31.1	189.8	189.8	55.0	511.4	247.8	587.5	310.1	53.2	345.2	63U.Y	537.0	317.9	280.8	527.8	353.3	382.3	364.4	582.3 68.6	204.1	225.7	495.5	228.1	351.7	313.9	291.9	1401	233.7	168.9	363.7	18.0	44.3	218.2	401.9	357.0	306.6	445.3	461.8
	8	781	783	784	785	787	788	700	161	792	793	794	267	797	798	199	801	802	803	804 804	806	807	808	808	810	811 812	813	814	815	816	818	819	820	821	823	824	825	827	828	829	830	831 837	833	834	835	836	838 838	839	840	841	843	844	845

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U - B	0.25	0.32	0.26	0.63	0.07	0.13	0.29	0.23	0.33	0.35	0.32	0.21	0.30	0.35	0.27	0.96	0.26	0.25	1.32	0.33	0.27	0.27	0.85	75.0	0.21	0.28	0.48	0.42	0.32	0.26	0.26	0.67	0.29	0.25	0.38	0.34	0.35	-0.43	0.15	0.36	0.32	0.11	0.80	0.29	0.41	0.26	1.43	0.39	0.69	1.31	0.35	0.33
B - V	0.87	0.93	0.91	0.87	0.81	0.84	0.92	0.95	0.76	0.80	0.87	0.91	0.92	0.87	0.82	1.11	0.93	0.88	1.3	1.00	0.91	0.91	1.05	0.83	0.00	06.0	0.93	0.84	1.02	3 2	0.86	2.28	0.87	0.93	0.92	0.97	0.92	0.33	0.89	0.89	0.0	0.85	0.84	0.96	191	0.90	1.33	0.91	1.11	U.32	0.92	0.92
Λ	19.35	19.35	19.35	19.35	19.35	19.35	19.36	19.36	19.36	19.37	19.38	19.38	19.38	19.38	19.39	19.39	19.39	19.39	19.40	19.40	19.41	19.41	19.41	19.42	19 42	19.42	19.42	19.42	19.42	19.43	19.43	19.43	19.43	19.44	19.44	19.44	19.45 19.45	19.45	19.45	19.46	19.47	19.47	19.47	19.47	19.47 10.48	19.48	19.48	19.48	19.49	19.49	19.49	19.49
Y	345.6	447.5	931.4	320.8	240.1	52.3 499.2	494.8	168.0	103.1	238.3 20.8	536.1	263.5	205.0	549.3 245 4	233.6	387.9	400.3	330.0	309.7	456.3	215.9	347.3	89.1	558.2	2 28	319.1	491.1	29.1	69.4 7 20 7	539.5 133 5	119.6	744.2	311.7	158.3	107.6	121.9	545.U	159.6	765.9	231.3	0.706	146.3	242.4	78.9	400.5	23.2	499.3	319.4	5.7	66.5	233.3	411.1
X	435.6	214.2	166.9	79.4	514.8	531.2 561.3	379.6	159.8	349.7	288.8	373.5	401.6	154.0	400.4	332.2	231.7	186.5	301.4	2.0.2	190.2	391.6	157.2	456.4	542.4	375 Q	449.5	598.8	395.0	191.7	30.5	84.6	41.0	360.5	403.8	166.3	488.8	10.2	409.0	186.0	219.6	424.8 86.2	34.6	38.3	617.0	624.7 420 £	110.3	548.7	482.9	314.4	610.4	349.5	305.1
8	1106	1107	1109	1110	1111	1112	1114	1115	1116	1117	1119	1120	1121	1122	1124	1125	1126	1127	1128	1130	1131	1132	1133	1134	1136	1137	1138	1139	1140	1141	1143	1144	1145	1147	1148	1149	1150	(2) 1152	1153	1154	1155	1157	1158	1159	1160	1162	1163	1164	1165	1167	1168	1169
U - B	0.24	0.47	0.34	0.32	0.65	0.28	0.31	0.33	0.58	0.24	0.25	0.34	0.43	0.25	0.20	0.30	0.24	0.35	0.24	0.23	0.25	0.20	0.52	0.24	65.0	0.31	0.27	0.26	0.21	0.95	0.16	0.66	0.52	0.26	0.30	0.55	0.27	0.56	0.22	0.29	0.43	0.48	0.30	0.54	0.30	0.48	0.41	0.36	0.21	0.25	0.16	0.19
B - V	0.88	1.01	89.0 680	0.88	1.02	0.92	0.84	0.89	0.85	0.88	0.87	0.87	0.97	0.88	0.90	0.90	0.93	1.07	0.89	0.92	0.89	0.91	0.97	0.93	16.0	0.80	0.87	0.91	0.87	1.10	0.90	1.01	0.91	0.88	0.89	0.90	0.92	1.06	0.89	0.90	0.1	1.07	0.91	0.97	0.88	0.62	0.92	0.89	0.85	0.93	0.95	0.93
Δ	19.22	19.23	19.23	19.24	19.24	19.24	19.24	19.24	19.24	19.25	19.25	19.26	19.26	19.26	19.26	19.27	19.27	19.27	19.27	19.27	19.27	19.28	19.28	19.28	19.28	19.28	19.29	19.29	19.29	19.29	19.29	19.30	19.30	19.30	19.31	19.31	19.31	19.32	19.32	19.32	19.32	19.32	19.33	19.33	19.33	10.33	19.33	19.34	19.34	19.34	19.34	19.34
۶	489.0	469.9	692.5	374.3	497.7	350.3	307.6	244.9	285.1	962.2 166 8	92.3	204.9	104.5	544.5	513.3 274 0	478.2	126.3	460.0	177.3	124.7	131.6	243.0	902.6	95.2	565.3	308.5	31.2	488.4	184.1	761.5	9.6 8.6	184.7	40.5	373.0	500.0	569.6	98.6 766.6	981.3	91.1	487.4	70.8	431.5	353.4	201.5	375.7	211.2	377.5	813.2	235.2	139.0	126.4	137.9
×	421.5	122.2	232.9	349.0	108.2	131.3	173.9	405.3	72.4	133.5	362.9	587.7	208.2	483.9	89.68	593.5	619.7	161.4	333.9	133.9	334.1	380.2	99.7	171.5	2.99.2	342.5	34.3	93.2	42.5	64.3 er e	154.1	467.9	293.7	407 1	445.3	557.0	179.4	1.101	311.9	358.8	625.4	90.2	250.0	544.3	446.6	0.016 165.6	295.1	296.1	369.3	475.4 175.1	129.4	200.8
B	1041	1042	1044	1045	1046	1047	1049	1050	1051	1052	1054	1055	1056	1057	1058	1060	1061	1062	1063	1065	1066	1067	1068	1069	0201	1023	1073	1074	1075	1076	1078	1079	1080	1081	1083	1084	1085	1087	1088	1089	1090	1092	1093	1094	1095	1097	1098	1099	1100	1102	1103	1104
																																											,									
U - B	0.45	0.17	0.43	0.28	0.29	0.80	0.35	0.45	0.32	0.45	0.22	0.14	0.17	0.57	0.18	0.17	0.70	0.55	0.22	0.20	0.32	0.22	0.58	0.25	00	0.18	0.20	0.21	0.26	0.16	0.19	0.41	1.33	0.32	0.14	0.12	0.61	0.21	0.20	0.57	0.50	0.33	0.35	0.19	0.16	0.61	0.34	0.25	0.20	0.41	0.18	0.38
B - V	0.92	0.97	1.4.1	0.86	0.87	1.12	06.0	1.03	0.86	0.69	0.85	0.85	0.82	0.95	0.85	0.87	1.03	0.85	0.92	0.91	0.92	0.88	0.86	0.88	0.04 0.0	0.89	0.85	0.81	0.70	0.88	0.87	1.20	1.56	0.82	0.86	0.80	0.99	0.89	0.89	0.96	4 90 0	0.84	0.94	0.87	0.86	0.61	06.0	0.94	0.88	0.90	0.89	0.91
2	19.11	11.01	11.91	19.11	19.11	19.11	19.12	19.12	19.12	19.12	19.13	19.13	19.13	19.13	19.14	19.14	19.14	19.14	19.14	19.14	19.14	19.14	19.14	19.14	1015	19.15	19.15	19.16	19.16	19.16	19.16	19.16	19.16	19.16	19.17	19.17	19.17	19.18	19.18	19.18	19.18	19.19	19.20	19.20	19.20	19.20	19.20	19.21	19.21	19.21	19.21	19.22
7	7.1	117.7	404.4 69.5	72.0	444.5	915.0 361.6	0.10C	137.5	57.2	85.9 430.5	5664.5	146.1	322.0	71.6	83.9	50.0	316.3	331.6	935.0 210 1	737.8	265.3	49.3	516.8	457.1	1.062	210.7	2.1	64.9	12.6	146.6	364.7	151.8	649.3	40.4 212.3	52.2	22.9	648.8 200.2	455.8	116.4	267.0	95.5 200 0	378.8	639.7	59.4	344.0	172.4	6.067	43.5	70.4	402.4	722.5	185.6
×	217.2	192.9	476.9	412.2	378.1	197.8	555.9	528.7	603.2	99.9 55.7	297.6	69.7	445.5	348.6	197.6	20.5	472.1	274.0	59.2	153.3	346.9	595.8	168.3	405.1	1.050	336.6	447.4	104.7	566.8	406.2	278.3	148.3	243.4	6.99.3	369.4	555.0	295.9	508.9	184.2	228.1	49.5 27K 7	149.6	16.8	235.3	334.9	582.0	76.4	548.6	437.4	441.1 613.2	372.2	502.7
A	976	970	876 676	086	981	982 083	984 984	985	986	987 988	68 6	066	991	992 002	993 994	395	966	660 2000	866	1000	1001	1002	1003	1004	1005	2001	1008	1009	1010	101	1013	1014	1015	1017	1018	1019	1020	1022	1023	1024	1025	1027	1028	1029	1030	1032	1033	1034	1035	1037	1038	1039

U - B	0.43	0.46	0.43	0.94	0.40	0.53	0.55	0.50
B - V	1.10	0.96	94	0.81	0.98	0.98	1.02	0.98
Λ	19.81	19.81	19.81	19.81	19.81	19.82	19.82	19.82
	9.0	3.1	9.5	1.8	6.3	8.4	1.9	2.0

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U - B	0.43	0.46	0.43	9 6.0	0.40	0.55	0.50	0.49	0.40 0.42	0.31	0.35	0.94	0.50	1.29	9-9- 9-7-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-	6.13 0.56	0.48	0.49	0.58	0.50	0.62		0.40	0.67	0.49	0.82	0.48	0.56	0.58	0.44	0.33	0.45	0.63	59.0 9 9	0.00	0.47	0.58	0.50	0.44	0.52	0.60	1.03	0.55	0.56	1.20	0.25	0.52	0.51	0.58	1.34	0.43	0.80	0.58	0.57	1 40
B - V	1.10	0.96	0.94	0.81	0.98 0.08	1.02	0.98	0.95	66'D	0.93	940	1.18	0.98	1.10	0.90	9 9 7 1	1.02	0.95	1.01	0.98	86.0	66.0 F	1.08	1.02	1.00	1.03	1.01	88	0.92	1.00	1.16	1.01	0.98	66.0	1 6.0	1.02	1.00	5	0.98	0.99	8.1	20.T	1.00	1.00	1.18	0.89	1.01	01.1 0.98	1.02	1.68	0.97	1.15	1.09	1.07	1 20
Δ	19.81	19.81	19.81	19.81	19.81	19.82	19.82	19.83	10.83	19.83	19.83	19.84	19.84	19.84	19.84	19.85 10 85	19.85	19.85	19.86	19.86	19.86	19.00	19.87	19.87	19.87	19.87	19.88	19.88	19.88	19.89	19.89	19.90	19.90	19.90	19.91	19.91	19.91	19.92	19.92	19.92	19.92	19.92	0.93	19.93	19.93	19.93	19.93	19.93	19.94	19.94	19.96	19.96	19.97	19.97	10.00
┝	340.6	183.1	589.5	351.8	336.3	31.9	422.0	594.5	128.5	573.1	894.2	238.0	500.1	510.6	317.9	142.8	715.1	415.5	444.4	651.0	518.2		120.5	128.8	619.0	245.7	261.0	373.9	50.1	363.8	5.3	524.8	134.1	300.8	17.3	182.2	559.2	292.7 800 6	74.1	385.0	413.5	2.96	280.9	49.7	598.2	194.7	776.2	705.4	540.1	270.9	61.4	417.6 468.2	827.4	169.4	7 400
×	479.7	413.3	355.8	172.8	282.0	629.0	355.0	568.9	341.1	182.9	207.5	182.9	451.2	520.2	127.2	135.8	26.6	303.2	569.7	125.4	265.0	0.410	136.4	362.7	294.0	295.5	599.8	1.1.1	272.2	290.0	75.6	83.5	626.0	110.1	249.9	424.8	524.0	258.0	444.9	191.7	507.2	195.9	486.6	343.8	575.0	306.1	186.8	103.5	339.0	69.3	62.3	322.6	120.1	547.0	4126
A	1301	1302	1303	1304	1305	1307	1308	1309	1310	1312	1313	1314	1315	1316	1317	1318	1320	1321	1322	1323	1324	0701	1327	1328	1329	1330	1331	1332	1333	1335	1336	1337	1338	1339	1341	1342	1343	1344 1246	1346	1347	1348	1349	1351	1352	1353	1354	1355	1357	1358	1359	1360	1361	1363	1364	1365
U = B	0.41	0.53	0.57	0.36	0.39	04.0	0.03	0.43	0.39	0.51	0.45	0.61	1.10	0.37	0.40	0.36	0.47	0.60	0.31	1.13	0.51	910	0.48	0.44	0.40	0.31	0.45	0.59	0.43	0.50	0.92	0.58	0.46	0.58	0.40	1.12	0.52	0.30	0.47	0.34	0.39	0.46	0.49	1.29	0.40	0.60	0.40	19.0	0.77	0.49	0.84	0.37	0.36	0.37	051
B = V	0.84	0.86	1.01	0.94	0.95	10.04 10.04	0.78	96 .0	16.0 18		0.95	0.96	1.14	1.06	0.98	0.90	1.13	1.03	1.01	1.20	0.97		000	0.95	0.97	0.90	0.98	1.04	0.95	0.A0	1.12	0.92	1.0	10.1	1.02	1.16	0.86	0.32	1.0	0.98	1.00	1.00	0.98 0.98	1.22	0.97	1.00	1.00	49.0 0 0 0	0.83	0.97	1.07	0.88	1.00	0.94	0.96
Δ	19.67	19.67	19.67	19.67	19.67	19.68	19.68	19.68	19.69 10.60	60.61	19.69	19.69	19.70	19.70	19.71	19.71	19.72	19.72	19.72	19.72	19.72	19.72	19.73	19.73	19.73	19.73	19.73	19.74	19.74	19.75	19.75	19.75	19.75	19.75	19.75	19.75	19.75	19.75	19.76	19.76	19.77	19.77	19.77	19.77	19.78	19.78	19.78	10.78	19.79	19.79	19.79	19.79	19.80	19.80	19.80
≻	435.6	116.1	740.0	645.7	238.6	280.9	366.5	532.1	75.3	517 3	534.5	228.5	289.7	485.6	491.4	566.1 460.0	18.4	962.9	118.2	875.7	442.4		802 Q	200.2	255.1	27.5	554.2	214.5	165.6	317.9	147.0	508.0	476.9	689.9	209.2	532.6	393.4	41.8	430.5	277.4	143.0	740.0	500.2 K24.8	867.7	593.5	623.8	150.9	175.2	100.1 96.5	45.4	315.5	527.4	154.1	130.6	202 5
×	138.0	249.8	166.2	280.2	386.3	362.3	323.4	339.2	449.3	- 00 20	580.2	611.8	25.0	213.9	250.1	202.6 79.5	184.8	107.5	453.0	90.4	483.3	1.010	808	313.3	399.5	102.4	260.8	86.6	338.5	117.8	370.4	368.0	619.7	391.9	0.000	370.0	245.0	439.5	526.6	393.7	334.5	174.7	13.7	246.5	255.5	391.1	261.9	90.2 427.6	498.5	608.0	585.2	347.9	199.3	89.3	536 9
e	1236	1237	1238	1239	1240	1242	1243	1244	1245	1247	1248	1249	1250	1251	1252	1263	1255	1256	1257	1258	1259	1201	1262	1263	1264	1265	1266	1267	1268	1209	1271	1272	1273	1274	1276	1277	1278	1279	1281	1282	1283	1284	1286	1287	1288	1289	1290	1291	1293	1294	1295	1296	1298	1299	1300
11 _ R	0.31	0.38	0.23	0.40	0.22	0.54	-0.9	0.35	0.34	07.0	- 0 - 70	0.38	0.58	0.43	0.38	0.89	0.80	0.46	0.39	0.53	0.56	0.33	1012	0.33	1.03	0.50	0.31	0.48	0.60	0.42	0.31	0.35	0.50	0.41	0.50 88 0	0.57	0.38	0.34	0.20	0.10	0.38	0.59	0.54	0.47	0.33	0.42	0.00	0.39	0.32	0.37	0.63	0.43	0.39	0.82	0.48
N Z	960	0.93	94	0.92	0.89	0.93	0.03	0.91	0.90	16.0	16.0 16.0	0.95	0.88	1.08	0.92	1.13	56.0 100	1.05	0.95	1.14	0.74	26.0	19.0	0.86	1.12	0.95	0.96	0.94	0.78	96.0 98.0	0.95	0.93	0.99	0.91	97 D	0.96	0.92	0.91	88.0	0.80	0.92	0.80	0.93	1.01	0.95	0.97	1.13	0.94 0.04	0.92 0.92	0.94	1.03	0.98	0.95	0.72	0000
1	19.49	19.49	19.50	19.50	19.50	19.5U	19.51	19.51	19.51	19.01	19.51	19.51	19.51	19.52	19.53	19.53	19.53	19.53	19.53	19.55	19.56	19.56	10.67	19.57	19.57	19.58	19.58	19.58	19.58	19.58	19.69	19.59	19.59	19.59	19.60	19.61	19.61	19.61	10.62	19.62	19.62	19.63	19.63	19.63	19.63	19.63	19.64	19.64	19.64	19.64	19.65	19.65	19.66 19.66	19.61	10.67
ŀ	4401	378.6	693.5	356.5	11.2	30.9	570.9	624.2	94.5	310.7	616.4	538.4	232.5	397.1	7.77	617.6	527.5	699.5	431.2	26.6	97.4	1.162	273.4	5.109	334.4	135.7	214.6	563.5	140.7	67.5	350.0	225.3	320.1	341.0	4 8.3	326.8	347.4	699.2	177.1	22.9	442.9	656.8	149.5	0770 166.2	393.4	9.5	179.2	638.4	736.7	804.7	188.4	639.3	82.5 6.7 F	170.3	166.4
ŀ	136.7	233.2	361.8	218.1	203.8	150.4	342.0	87.8	458.1	160.9	398.8	242.5	75.1	29.5	595.1	170.4	288.9	317.6	209.5	66.7	19.6	277.2	1/1/1	1.010	92.3	619.5	567.2	169.0	463.1	584.3	414 7	216.1	114.6	66.3	525.4	267.8	310.4	304.0	400.3	566.6	307.5	388.9	417.3	404.2	522.3	546.9	439.0	401.1	167.6	198.4	314.0	127.6	417.4 1941	1.501	216 6
E		1172	1173	1174	1175	1176	1178	1179	1180	1181	1183	1184	1185	1186	1187	1188	1189	1191	1192	1193	1194	1195	1196	1198	1199	1200	1201	1202	1203	1204	1205	1207	1208	1209	1210	1212	1213	1214	1215	1217	1218	1219	1220	1221	1223	1224	1225	1226	1227	1229	1230	1231	1232	1234	1235

a 11	0.76	1.59	0.80	0.63	1.41	1.00	0.69	1.57	0.78	1.092	0.75	0.71	0.72	1.40	0.66	0.83	0.87	0.80	0.74	0.09	0 76 0 76	1.38	0.92	0.72	0.74	0.45	16'N	0.73	0.34	0.83	0.81	0.75	0.68	0.81	0.89	1.42	0.67	0.83	0.65	0.66	16.0	0.85	0.87	0.88	0.79	0.87	0.37	0.95	1.10	1.25	0.82	1.64	0.75	
A a	113	1.166	1.09	1.02	1.45	101	1.04	1.47	1.09	0.64	0.97	1.10	1.10	0.47	1.12	311	ITI	1.11	1.08	0.85	101	1.58	1.00	1.12	1.16	0.98	1.02	1.31	0.96	1.15	7 1.24	1.09	1 128	1.04	1.09	0.73	101	1.16	1.24	1.09	1.09	1 1.16	1.12	1.01	1.12	1.09	96.0 H	1.09	1.15	1.25	1.11	0.90	1.01	000
Å	20.26	20.36	20.36	20.36	20.37	20.38	20.38	20.38	20.38	20.39	20.39	20.40	20.40	20.41	20.41	20.42	20.42	20.42	20.43	20.43	20.43	20.44	20.45	20.45	20.45	20.46	20.4t	20.46	20.46	20.47	20.47	20.48	20.48	20.49	20.49	20.50	20.50	20.51	20.51	20.51	20.52	20.53	20.53	20.53	20.54	20.54	20.54	20.55	20.55	20.55	20.55	20.55	20.50	
Ņ	3441	579.7	976.1	618.9	483.5	820.1	714.8	132.7	402.4	416.0	631.4	174.6	761.2	163.4	512.8	765.9	598.6	270.6	194.1	908.0	115.2	161.4	603.3	633.8	110.4	302.7	92.9	143.0	408.2	249.1	208.0	376.7	135.9 815.9	221.5	614.2	68.4	568.9	962.0	146.5	42.2	362.6	294.9	513.3	331.4	232.2	643.8	125.0	219.4	403.4	415.6	250.6	509.7	857.7	
ŀ	136.2	28.8	59.5	566.6	322.7	127.7	108.3	490.5	498.0	100.0	128.3	305.6	123.8	274.1	230.7	198.4	636.3	246.5	520.0	73.1	12.8	549.6	105.9	326.8	419.9	384.0	466.8	3/0.0	437.4	205.1	472.7	621.4	185.4	341.4	266.5	498.8	43.8	162.3	263.8	329.8	\$.002 69.8	48.0	304.9	63.3 535 4	509.5	330.1	425.6	382.5	595.6	19.5	585.6	165.0	170.9	0.001
E	1406	1497	1498	1499	1500	1502	1503	1504	1505	1507	1508	1509	1510	1511	1512	1514	1515	1516	1517	1518	1610	1521	1522	1523	1524	1525	1520	1528	1529	1530	1531	1532	1533	1535	1536	1537	1535	1540	1541	1542	1544	1545	1546	1547	1549	1550	1551	1552	1554	1555	1556	1557	1555	
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2	1 1 0	0.57	0.49	0.60	1.41	0.61	0.60	0.58	0.50	0.67	0.73	0.09	0.74	0.87	0.71	L. 20	0.35	0.95	0.73	0.69	0.650	0.86	0.56	0.94	0.66	1.01	0.63	16.0	0.38	1.30	0.65	0.82	0.49	1.06	0.79	0.97	1.25	0.71	0.79	0.25	1.05	1.44	0.78	0.70	0.68	0.42	0.88	0.62	0.74	0.68	0.78	0.76	0.74	
14 0	1 60	1.04	0.96	1.00	1.53	1.06	1.06	1.09	1.03	1 08	0.99	0.81	1.14	1.01	1.05	1.05	0.80	1.21	1.08	1.08	00.T	1.00	1.08	0.56	1.14	1.16	1.05	1.01	1.25	1.24	1.08	0.75	0 1 1	1.29	1.15	1.22	1.04	1.05	1.02	0.76	8 I	1.34	1.06	1.16	0.90	0.95	1.09	1.01	0.84 1.07	1.01	1.09	1.10	1.02	
1	20.17	20.17	20.17	20.17	20.18	91.02	20.19	20.19	20.19	20.20	20.20	20.21	20.21	20.21	20.21	20.22	20.22	20.23	20.23	20.24	20.24	20.25	20.25	20.25	20.25	20.26	20.26	20.27	20.27	20.27	20.27	20.27	20.27	20.27	20.27	20.28	90.02	20.29	20.29	20.30	20.30	20.30	20.30	20.31 20.31	20.32	20.33	20.33	20.33	20.34	20.34	20.34	20.35	20.35	
>	101	700 5	455.8	128.4	259.4	940.9 606.5	202.3	57.7	383.1	215.0	369.8	270.6	121.4	187.0	572.8	29.1	400.1	450.5	625.5	460.2	971.0	135.2	292.2	368.2	194.8	35.1	260.7	30U.0	89.1	608.5	169.3	910.6	171.6	228.4	815.2	633.6	59.3 703 5	537.0	371.8	414.2	506.5	513.2	653.5	105.7 325.4	303. * 616.0	868.5	710.2	825.2	299.2 581.3	513.5	494.9	83.6	306.4	
ļ	1631	1.601	539.0	556.5	488.3	508 K	351.7	334.7	178.4	240.9 565 0	208.7	481.7	613.2	291.5	459.5	469.8	125.1	523.6	557.6	377.7	2603C	304.9	424.6	98.2	250.3	339.1	423.6	170.1	243.0	95.3	329.4	213.8	632.1 261 0	490.3	210.3	635.0	50.9	293.8	335.4	512.8	380.2	285.6	341.5	628.0	137.8	229.3	186.0	36.8	305.7	335.3	484.6	315.2	309.9	
f	1421	1432	1433	1434	1435	1427	1438	1439	1440	1441	1443	1444	1445	1446	1447	1449	1450	1451	1452	1453	1454 1466	1456	1457	1458	1459	1460	1461	1463 1463	1464	1465	1466	1467	1468	1470	1471	1472	1474	1475	1476	1477	1479	1480	1481	1482	1484	1485	1486	1487	1489	1490	1491	1492	1493	
a 11	200	0.56	0.21	0.51	0.52	1.13	0.54	0.88	0.66	0.20	1.14	0.09	0.45	0.59	1.1	0.02	0.04	0.59	1.28	0.34	0.71	0.60	0.97	0.53	0.55	0.47	0.52	0.56	0.66	0.35	0.94	0.61	0.16	0.71	0.74	0.54	0.30	0.69	0.49	0.64	0.62	0.76	1.20	0.65	0.46	0.20	0.77	0.32	0.00 0 70	0.64	0.54	1.16	0.60	
11 0	100	0.00 86 0	0.88	0.99	1.05	1.23	0.99	1.15	0.99		1.24	0.82	0.92	0.98	1.23	1.08	0.69	0.99	1.38	1.23	1.03	1.04	1.07	1.09	1.06	1.29	1.12	90 F	1.05	0.91	1.39	1.00	0.98	0.92	1.02	1.02	0.92	0.96	1.01	1.06	1.00	0.98	1.32	1.07	0.96	0.84	1.14	0.91	1.10	1.06	1.08	1.21	1.09	
1	10.00	10 08	19.99	19.99	19.99	10 00	19.99	19.99	19.99	20.00	20.01	20.01	20.01	20.02	20.02	20.02	20.04	20.04	20.04	20.04	20.04	20.05	20.06	20.06	20.06	20.06	20.07	20.07	20.08	20.08	20.08	20.09	20.10	20.10	20.11	20.11	20.11	20.11	20.11	20.11	20.12	20.12	20.12	20.12	20.13	20.14	20.14	20.15	20.15 20.15	20.16	20.16	20.16	20.16	
,	160.01	0.201	555.5	643.3	438.9	2007 S	194.1	942.8	204.3	032.3 208 0	461.6	123.1	682.0	118.0	2.7	88. 1 749.6	147.5	227.6	734.4	71.6	57.9	90F.2	26.5	110.5	938.9	249.6	638.7	4710	104.1	514.8	404.4	28.8	293.0	249.5	512.2	908.0	440.6 K22.0	140.0	475.1	712.9	314.2	6.3	439.5	555.0	497.1	49.6	533.0	367.7	349.6 451 4	733.7	957.9	611.5	197.1	
>	< 10	512.0	17.5	454.1	499.9	517.8 234.6	496.5	120.5	221.8	334.0 1171	218.0	346.6	164.7	98.5	568.7	919.9	532.2	404.8	144.1	248.0	525.3 161 0	90.4	335.0	137.3	29.7	157.2	105.2	405.4 228.2	295.7	413.4	86.4	236.5	241.1	28.8	389.9	187.4	264.4	306.9	210.0	128.2	163.5	126.4	202.7	240.3	537.1 608.3	322.0	215.3	46.8	519.1	108.9	138.9	275.1	195.3	
	200	1367	1368	1369	1370	1371	1373	1374	1375	1377	1378	1379	1380	1381	1382	1384	1385	1386	1387	1388	1300	1391	1392	1393	1394	1395	1396	1397	1399	1400	1401	1402	1403	1405	1406	1407	1400	1410	1411	1412	1414	1415	1416	1417	1419	1420	1421	1422	1423	1425	1426	1427	1428	

469 HODDER ET AL.: PHOTOMETRY AND VARIABLE STARS IN M71

	1	V V	B = V	U - B	ID 1626	X 397.8	Y 385.4	V 20.78	B - V 1.06	U – B 1.14	1691	X 435.9	Y 627.0	V 21.07	B - V 1.14	U = B 1.47
0.00 <td< td=""><td>.4 20.58 .6 20.58</td><td>~ ~</td><td>1.10</td><td>0.90</td><td>1625</td><td>25.3</td><td>360.1 498.5</td><td>20.78</td><td>0.96</td><td>1.26</td><td>1692</td><td>337.0</td><td>358.6</td><td>21.07</td><td>1.13</td><td>1.52</td></td<>	.4 20.58 .6 20.58	~ ~	1.10	0.90	1625	25.3	360. 1 498.5	20.78	0.96	1.26	1692	337.0	358.6	21.07	1.13	1.52
Male 11, 12, 13, 14, 14, 14, 14, 14, 14, 14, 14, 14, 14	.9 20.58		0.99	0.39	1628	395.8	459.3	20.79	1.76	0.93	1693	39.2	379.0	21.08	1.28	1.09
100 <td></td> <td></td> <td>1.04</td> <td>0.73</td> <td>1629</td> <td>444.8 212.0</td> <td>157.8</td> <td>20.79</td> <td>1.20</td> <td>0.87</td> <td>1695</td> <td>313.8</td> <td>230.2</td> <td>21.10</td> <td>1.19</td> <td>1.09</td>			1.04	0.73	1629	444.8 212.0	157.8	20.79	1.20	0.87	1695	313.8	230.2	21.10	1.19	1.09
100 <td>.9 20.59</td> <td></td> <td>1.04</td> <td>66.0</td> <td>1631</td> <td>156.9</td> <td>382.4</td> <td>20.80</td> <td>1.06</td> <td>1.70</td> <td>1696</td> <td>237.6</td> <td>140.0</td> <td>21.11</td> <td>1.40</td> <td>0.89</td>	.9 20.59		1.04	66.0	1631	156.9	382.4	20.80	1.06	1.70	1696	237.6	140.0	21.11	1.40	0.89
111 111 112 <td>(.3 20.59</td> <td>~ ·</td> <td>0.80</td> <td>1.29</td> <td>1632</td> <td>12.9</td> <td>610.9</td> <td>20.81</td> <td>1.22</td> <td>1.11</td> <td>1697</td> <td>524.7 461 0</td> <td>434 1</td> <td>21.11</td> <td>0.45</td> <td>2.19</td>	(.3 20.59	~ ·	0.80	1.29	1632	12.9	610.9	20.81	1.22	1.11	1697	524.7 461 0	434 1	21.11	0.45	2.19
1.08 0.03 0.04 <th0.04< th=""> 0.04 0.04 <th0< td=""><td>.5 20.60</td><td></td><td>1.08</td><td>0.85</td><td>1634</td><td>436.2</td><td>184.6</td><td>20.83</td><td>1.38</td><td>1.03</td><td>1699</td><td>324.6</td><td>403.0</td><td>21.12</td><td>1.23</td><td>1.18</td></th0<></th0.04<>	.5 20.60		1.08	0.85	1634	436.2	184.6	20.83	1.38	1.03	1699	324.6	403.0	21.12	1.23	1.18
	9 20.60		1.08	0.83	1635	84.0	312.7	20.84	1.1	0.73	1700	53.5	677.3	21.12	1.27	1.17
0.000 <th< td=""><td>1.5 20.60</td><td>~ ^</td><td>1.04</td><td>1.08</td><td>1636</td><td>445.7 750 0</td><td>589.5 610 1</td><td>20.85</td><td>17.1</td><td>1.74</td><td>12021</td><td>377.5</td><td>209.9</td><td>21.14</td><td>1.25</td><td>1.58</td></th<>	1.5 20.60	~ ^	1.04	1.08	1636	445.7 750 0	589.5 610 1	20.85	17.1	1.74	12021	377.5	209.9	21.14	1.25	1.58
117 0.07 117 0.07 117 0.03 11.0 0.03 11.1 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.	20.60		0.95	0.12	1638	228.0	396.1	20.85	1.37	1.33	1703	285.0	719.2	21.14	1.20	1.23
113 0.07 1640 311.8 0.05 0.04 <th< td=""><td>.1 20.61</td><td></td><td>1.17</td><td>0.82</td><td>1639</td><td>596.6</td><td>285.9</td><td>20.85</td><td>1.20</td><td>0.97</td><td>1704</td><td>541.1</td><td>399.3</td><td>21.15</td><td>1.14</td><td>1.31</td></th<>	.1 20.61		1.17	0.82	1639	596.6	285.9	20.85	1.20	0.97	1704	541.1	399.3	21.15	1.14	1.31
11.0 0.06 1041 2011 2025 11.0 0.000 2012 21.0 11.0 0.000 21.0 11.0 11.0 0.000 21.0 11.0	.2 20.61	_	1.12	0.87	1640	331.8	301.6	20.86	1.12	1.07	1705	320.7	82.9	21.16	1.22	1.17
1111 0.09 1004 <th< td=""><td></td><td></td><td>1.19</td><td>0.96</td><td>1641</td><td>291.1</td><td>189.2</td><td>20.80</td><td>1.13</td><td>76.0</td><td>2021 00/T</td><td>1.102</td><td>2002</td><td>01.12</td><td>1.25</td><td>1 23</td></th<>			1.19	0.96	1641	291.1	189.2	20.80	1.13	76.0	2021 00/T	1.102	2002	01.12	1.25	1 23
11/1 0.00 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 0.01 11/1 11/1 0.01 11/1 <th< td=""><td>1.7 20.62</td><td>~ ~</td><td>1.16</td><td>96.0</td><td>1642</td><td>510.4</td><td>132.3</td><td>20.88</td><td>1.54</td><td>1.30</td><td>1708</td><td>238.5</td><td>417.6</td><td>21.19</td><td>1.58</td><td>1.49</td></th<>	1.7 20.62	~ ~	1.16	96.0	1642	510.4	132.3	20.88	1.54	1.30	1708	238.5	417.6	21.19	1.58	1.49
110 0.00 1046 0.000 0.0	4 20.62	• ~	1.17	62.0	1644	480.0	407.7	20.88	1.03	1.39	1709	504.1	341.9	21.20	1.63	1.17
111 0.05 1647 0660 6477 7000 1104 0600 1111 64.0 04.00 1111 64.0 04.00 1111 64.0 04.00 1111 64.0 04.00 1111 1111 64.0 04.00 1111 1111 64.0 11111 11111 11111	1.1 20.62	~	1.09	0.85	1645	100.6	869.6	20.88	1.10	0.83	1710	390.1	32.6	21.23	1.07	1.16
111 0.00 1684 40.01 40.01 10.	0.0 20.63	~	1.19	0.85	1646	566.0	647.7	20.89	1.06	0.98	1171	434.2	576.9	21.23	1.09	0.99
1111 0.00 <th< td=""><td>.9 20.63</td><td></td><td>1.15</td><td>0.90</td><td>1647</td><td>305.4</td><td>475.1</td><td>20.89</td><td>1.14</td><td>1.40</td><td>21/1</td><td>348.0 2.20 K</td><td>305.2</td><td>21.24</td><td>1 ¥ 1</td><td>5.5</td></th<>	.9 20.63		1.15	0.90	1647	305.4	475.1	20.89	1.14	1.40	21/1	348.0 2.20 K	305.2	21.24	1 ¥ 1	5.5
11.0 0.00 1000 1000 1010 0.01 1010 0.01 1010 0.01 1010 0.01 1010 <th< td=""><td>1.2 20.63</td><td></td><td>111</td><td>0.95</td><td>1649</td><td>182.5</td><td>617.8</td><td>20.90</td><td>1.54</td><td>1.13</td><td>1714</td><td>445.3</td><td>445.0</td><td>21.26</td><td>1.54</td><td>1.20</td></th<>	1.2 20.63		111	0.95	1649	182.5	617.8	20.90	1.54	1.13	1714	445.3	445.0	21.26	1.54	1.20
0.00 0.01 <th0.01< th=""> 0.01 0.01 <th0< td=""><td>20.63</td><td></td><td>1.16</td><td>06.0</td><td>1650</td><td>243.5</td><td>55.9</td><td>20.90</td><td>1.25</td><td>1.01</td><td>1715</td><td>99.7</td><td>338.8</td><td>21.26</td><td>1.10</td><td>1.03</td></th0<></th0.01<>	20.63		1.16	06.0	1650	243.5	55.9	20.90	1.25	1.01	1715	99.7	338.8	21.26	1.10	1.03
1.00 0.91 1.652 2333 65.5 20.90 1.718 56.5 21.27 1.21 0.03 1.10 0.96 1653 74.5 35.3 55.7 50.90 1.718 56.5 21.47 1.21 0.19 1.10 0.96 1655 70.44 50.35 1.05	.5 20.64		0.26	0.57	1651	151.2	171.8	20.90	1.30	1.05	1716	282.7	329.3	21.26	1.30	0.88
1.26 1.26 1.26 1.26 1.26 1.27 1.26 1.26 2.24 <th2.24< th=""> 2.24 2.24 <th2< td=""><td>.9 20.64</td><td>-</td><td>1.09</td><td>0.91</td><td>1652</td><td>233.3</td><td>65.6</td><td>20.90</td><td>1.11</td><td>0.82</td><td>1717</td><td>558.2</td><td>66.5</td><td>21.26</td><td>1.37</td><td>0.99</td></th2<></th2.24<>	.9 20.64	-	1.09	0.91	1652	233.3	65.6	20.90	1.11	0.82	1717	558.2	66.5	21.26	1.37	0.99
1.00 1.10 1.00 <th< td=""><td>1.8 20.64</td><td>-</td><td>1.25</td><td>1.98</td><td>1653</td><td>244.5</td><td>353.7</td><td>20.91</td><td>1.29</td><td>0.99</td><td>1718</td><td>549.6 7E 0</td><td>234.4</td><td>21.27</td><td>0.88</td><td>0.17</td></th<>	1.8 20.64	-	1.25	1.98	1653	244.5	353.7	20.91	1.29	0.99	1718	549.6 7E 0	234.4	21.27	0.88	0.17
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3 20.64	-	1.09	1.16	1654 1666	14.2 K20 R	80.8	20.92	1.22	1.04	1720	315.8	664.3	21.27	1.22	60.1
111 0.01 1657 3044 3145 0.09 133 0.07 0.08 133 0.09 133 0.09 133 0.05 134 136 0.05 134 137 134 131 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134 134	1.5 20.65 8 20.66	o "	118	0.96	1656	350.1	363.4	20.93	1.24	1.16	1721	213.5	687.6	21.27	1.13	1.20
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$.4 20.66		1.21	0.81	1657	208.4	334.6	20.94	1.32	0.87	1722	537.9	597.5	21.27	0.83	0.13
116 0.89 1659 4454 7.20 1.24 1.25 31.4 1.25 31.4 1.25 1.24 1.25 <th1< td=""><td>1.2 20.66</td><td>ŝ</td><td>1.18</td><td>0.96</td><td>1658</td><td>246.7</td><td>134.3</td><td>20.94</td><td>1.43</td><td>0.69</td><td>1723</td><td>87.7</td><td>751.9</td><td>21.28</td><td>1.15</td><td>0.83</td></th1<>	1.2 20.66	ŝ	1.18	0.96	1658	246.7	134.3	20.94	1.43	0.69	1723	87.7	751.9	21.28	1.15	0.83
0.00 <th< td=""><td>.7 20.67</td><td>~ •</td><td>1.16</td><td>0.89 25 0</td><td>1659</td><td>401 8</td><td>171.8 607.8</td><td>20.95</td><td>1.31</td><td>1.10</td><td>1725</td><td>391.4</td><td>459.9</td><td>21.29</td><td>1.30</td><td>1.30</td></th<>	.7 20.67	~ •	1.16	0.89 25 0	1659	401 8	171.8 607.8	20.95	1.31	1.10	1725	391.4	459.9	21.29	1.30	1.30
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	20.68		0.86	1.40	1661	324.4	389.9	20.95	1.09	1.24	1726	32.9	173.4	21.30	1.36	1.21
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$.4 20.68) an	1.11	2.45	1662	350.6	208.5	20.95	0.67	1.53	1727	581.3	423.7	21.30	0.52	0.00
0.97 0.80 1564 37.01 80.03 1.05 <	0.6 20.68	80	1.23	06.0	1663	400.9	416.1	20.96	0.97	1.13	1728	551.3	85.9	21.30	1.62	1.62
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$.8 20.69	ወሳ	0.97	0.80	1664 1665	20.1	351.2	20.96	1.19	1.20	1730	65.8	111.4	21.31	1.07	1.24
114 123 1667 388, 112,6 20.97 113 114 1732 362.1 410.3 21.33 107 0.03 0.86 0.10 1667 386.3 215.3 20.97 101 0.66 11735 519.6 56.00 21.33 107 0.65 1.28 166 1677 56.0 77.33 20.99 1.10 0.66 11.735 519.6 56.5 21.33 0.77 26.1 47.1 26.1 27.3 1.24 1.26	4 20.69	"	1.10	0.77	1666	259.9	492.5	20.97	1.30	1.27	1731	491.0	242.2	21.32	1.44	1.21
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1.6 20.69	ስ ወ	1.14	1.23	1667	298.4	112.6	20.97	1.13	1.14	1732	362.1	410.3	21.32	1.00	0.36
0.96 0.04 1573 1563 0.01 1735 1534 9034 1331 133 <t< td=""><td>.9 20.70</td><td>0</td><td>1.01</td><td>0.85</td><td>1668</td><td>336.3</td><td>215.3</td><td>20.97</td><td>1.01</td><td>0.66</td><td>1733</td><td>619.6</td><td>636.U</td><td>21.33</td><td>1.01</td><td>0.62</td></t<>	.9 20.70	0	1.01	0.85	1668	336.3	215.3	20.97	1.01	0.66	1733	619.6	636.U	21.33	1.01	0.62
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	20.70	_	8.0	1 10	1670 1670	267.6	776.6	20.98	0.83	0.01	1735	103.4	492.8	21.33	1.36	1.21
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	20.71		1.38	1.66	1671	446.2	429.7	20.99	1.10	0.75	1736	260.1	36.7	21.35	1.30	1.02
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$.2 20.71		1.28	1.48	1672	65.0	737.3	20.99	1.25	1.12	1737	514.0	255.8	21.35	1.35	1.15
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$.9 20.71	-	1.20	1.07	1673	438.8	323.3	20.99	1.23	1.13	1738	33.0	693.3	21.35	1.20	0.99
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.9 20.73	m –	1.10	1.03	1674	52.8	403.3	66.02	1 0.7	77.1	601T	0.00 L 99.0	102.2	10.12	0.1	1.03
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.8 20.73	m	1.18	1.10	1675	471.5	2467.0	66.02	1.44	01.1	1741	7.00 90 09	0.000	10.12	115	1 10
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1 20.73	m •	1.13	1.07	1676	337.9 60.6	416.8	20-17 51 00	1.15	1.60	1742	544.3	616.2	21.38	1.27	1.70
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	51.02 T.	n -	01-1 01-1	60'T	1678	237.6	489.4	21.00	1.23	1.33	1743	64.7	349.2	21.40	1.29	1.40
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10 20 27		961	1.06	1679	115.7	128.5	21.00	1.23	0.82	1744	226.4	563.4	21.41	1.35	1.38
	20.74		0.95	1.43	1680	397.9	198.9	21.01	0.70	0.75	1745	334.9	674.4	21.42	1.01	0.22
114 1.05 1682 384.5 384.2 21.01 1.22 1.28 1747 130.1 737.7 21.43 1.30 0.47 1.47 1.27 1.683 564.1 566.2 21.03 1.14 1.35 1.36 1.37 1.31 1.37 1.31 1.32 1.31 1.31 1.32 1.31 1.31 1.32 1.31 1.31 1.31 1.31 1.31 1.31 1.31 1.31 1.31 1.31 1.32 1.31 1.32 1.33 1.33	.4 20.74		1.21	1.18	1681	212.4	164.4	21.01	1.15	0.39	1746	514.0	177.3	21.43	0.52	0.82
1.47 1.27 1.683 56.41 56.5 21.03 1.14 1.35 1749 1833 1634 57.3 1.37 1.40 1.54 1.55 1.684 57.3 55.64 56.62 21.03 1.37 1.40 1.54 1.55 1.684 57.3 55.71 21.43 1.37 1.40 1.54 1.45 1.68 37.79 55.74 21.04 1.23 0.84 1770 326.9 55.71 21.44 1.38 1.35 1.26 1.35 1.10 1.13 1.73 36.9 55.71 21.44 1.38 1.36 1.26 1.55 1.16 1.13 1.71 1.71 1.37 1.26 1.27 0.89 1.668 34.6 21.05 1.16 1.13 1.73 1.26 1.07 1.29 1.668 1.83 64.9 2.106 1.51 1.73 1.74 1.43 1.44 1.44 1.44 <t< td=""><td>1.1 20.74</td><td></td><td>1.14</td><td>1.05</td><td>1682</td><td>364.6</td><td>384.2</td><td>21.01</td><td>1.22</td><td>1.28</td><td>1747</td><td>130.1</td><td>737.7</td><td>21.43</td><td>1.10</td><td>0.47</td></t<>	1.1 20.74		1.14	1.05	1682	364.6	384.2	21.01	1.22	1.28	1747	130.1	737.7	21.43	1.10	0.47
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1.2 20.75	١O	1.47	1.27	1683	564.1	566.2	21.03	1.14	1.35	1748	383.9	163.6	21.43	1.37	1.31
1.54 1.45 1.66 0.83.73 2.53.4 2.1.05 1.1.3 1.03 1.03 2.1.44 1.43 1.33 1.34 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.34 1.33 1.33 1.34 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1.34 1.44 1.43 1.44 1.43 1.44 1.43 1.44 1.43 1.44 1.43 1.43 1.73 1.75 5.03 330.3 2.144 1.43 1.74 1.74 1.74 1.44 1.44 1.44 1.44 1.44 1.44 1.44 1.44 1.44 1.44 1.74	1.2 20.75	۰C	1.27	0.92	1684	573.9	587.8	21.03	1.23	0.96	1749	124.9	858.2	21.43	1.37	1.16
1.20 1.30 1.00 1.45 1.13 1.75 6.03 3.03 2.144 1.48 1.44 1.22 0.39 1667 20.8 34.6 1.10 1.15 1.75 6.03 33.03 2.144 1.48 1.44 1.07 1.20 1668 18.3 64.92 21.06 1.50 1.51 1753 510.0 6.37 21.46 1.37 1.74 1.07 1.20 1668 18.3 64.92 21.06 1.50 1753 510.8 21.46 1.37 1.74 1.07 1.68 1.53 1670 1.50 1.51 1.77 1.37 1.74 1.10 1.07 1669 1.52 1.06 1.50 1.74 1.25 1.37 1.74 1.10 1.07 1689 1.52 1.06 1.50 1.74 1.26 1.37 1.10 1.07 108 34.46 2.1.49 1.26 1.37	1.4 20.75	io i	1.54	1.45	1685	327.9	263.4	21.04	1.15	1 10	1751	97.025	557.1 686 5	21.44	1.38	1.26
1.07 1.00 1688 18.3 649.2 21.06 1.50 1.51 1753 519.0 63.7 21.45 1.37 1.74 1.10 1.07 1.60 15.1 1.17 0.83 1754 208.8 244.6 21.49 1.25 1.37 1.10 1.07 1689 15.2 167.8 21.06 1.17 0.83 1754 208.8 244.6 21.49 1.25 1.37 1.11 1.01 1.07 1.08 0.28 1755 453.6 748.2 21.49 1.26 1.37 1.15 1.03 1690 333.8 691.2 21.07 0.96 0.28 1755 453.6 74.82 21.49 1.60 1.84	20.76		1.46	1.35	1687	20.8	34.6	21.05	1.45	1.13	1752	620.3	330.3	21.44	1.48	1.44
7 1.10 1.07 1689 15.2 167.8 21.06 1.17 0.83 1754 208.8 244.6 21.49 1.25 1.37 1 1.15 1.03 1690 333.8 691.2 21.07 0.96 0.28 1755 453.6 748.2 21.49 1.60 1.84	20.73		1.07	1.20	1688	18.3	649.2	21.06	1.50	1.51	1753	519.0	63.7	21.45	1.37	1.74
1.15 1.03 1690 333.8 691.2 21.07 0.96 0.28 1755 453.6 748.2 21.49 1.60 1.84	22.07 c.			1.07	1689	15.2	167.8	21.06	1.17	0.83	1754	208.8	244.6	21.49	1.25	1.37
	1.3 20.78		1.15	1.03	1690	333.8	691.2	21.07	0.96	0.28	1755	453.6	748.2	21.49	1.60	1.84

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1756 23.46 51.01 21.46 1.26 1.26 1.26 23.20 176 75.1 75.1 75.1 1.26 1.26 1.26 23.64 20.65 23.11 176 75.1	Ð	×	٠¥	Λ	B - V	U - B	Ð	x	Y	Λ	B - V	U - B
177 77.3 77.3 77.3 77.3 77.4	1756	224.6	261.0	21.49	1.42	1.14	1821	197.4	353.5	22.09	1.16	1.35
1738 75.1 70.2 21.1 1.46 1.38 19.23 96.0 21.1 1700 41.7 66.0 21.81 1.41 19.85 50.6 21.21 21.12 21.11 1701 41.17 66.0 21.81 1.00 27.2 22.2 1768 60.65 21.81 1.00 1.81 18.95 50.01 21.12 21.2 1768 60.65 21.81 1.70 1.81 18.95 50.01 21.2 22.2 1770 21.43 60.65 21.61 1.11 1.81 1.85 22.2 22.2 1770 21.43 60.65 21.61 1.11 1.81 1.82 22.4 22.4 1770 21.43 1.71 1.71 1.81 1.71 22.2 22.2 22.4 21.4 22.4 22.4 22.4 22.4 22.4 22.4 22.4 22.4 22.4 22.4 22.4 22.4 22.4	1757	217.8	873.1	21.50	1.42	1.22	1822	87.5	894.4	22.09	1.31	1.38
1709 382.4 51.2 21.51 1.41 1.46 182.4 182.4 157.3 22.11 1709 388.4 57.5 21.51 1.14 1.46 182.4 159.4 37.3 22.11 1703 10.08 77.4 21.51 1.14 1.46 182.8 316.1 22.12 1704 10.08 77.4 1.51 1.01 1.41 1.46 1.81.8 1.31.2 22.23 1776 310.3 515.6 1.51 1.51 1.51 1.51 22.23 22.23 1777 310.1 310.3 1.51 1.51 1.51 22.23 22.23 1777 310.1 310.3 1.51 1.11 0.77 22.23 22.23 1777 310.1 310.1 1.21 1.21 1.21 22.23 1777 310.1 310.1 1.21 1.21 1.21 22.23 1777 310.1 310.1 310.1 310.1	1758	75.1	702.5	21.51	1.36	1.28	1823	94.2	866.0	22.11	1.40	1.35
Ifo Hir 551.9 215.1 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.04 <th< td=""><td>1759</td><td>388.8</td><td>352.2</td><td>21.51</td><td>1.41</td><td>1.46</td><td>1824</td><td>100.2</td><td>572.5</td><td>22.11</td><td>0.85</td><td>1.07</td></th<>	1759	388.8	352.2	21.51	1.41	1.46	1824	100.2	572.5	22.11	0.85	1.07
110 37.1 50.0 21.2 0.4.1 0.4.	1760	481.7	561.9	21.51	0.83	0.28	1825	589.4	37.3	22.11	1.54	10.1
Time <th< td=""><td>1011</td><td>1.12</td><td>0.100</td><td>71.02</td><td>1.42</td><td>1.14</td><td>10791</td><td>139.0</td><td>1.115</td><td>71.77</td><td>1.01</td><td>8.1</td></th<>	1011	1.12	0.100	71.02	1.42	1.14	10791	139.0	1.115	71.77	1.01	8.1
177 177 178 178 118 117 127 127 127 127 127 127 127 127 128 <td>1763</td> <td>110.8</td> <td>757 4</td> <td>21.52</td> <td>140</td> <td>138</td> <td>1828</td> <td>315.1</td> <td>310.5</td> <td>22.15</td> <td>1.64</td> <td>1.51</td>	1763	110.8	757 4	21.52	140	138	1828	315.1	310.5	22.15	1.64	1.51
17.05 44.6 36.05 21.53 111 0.81 188.0 54.2 22.20 17.06 54.9 36.05 21.55 1.70 11.7 188.1 18.6 64.8 22.20 17.06 21.45 1.40 1.11 1.13 1.13 52.33 22.33 17.70 21.43 64.93 21.46 1.13 1.23 22.33 22.33 17.70 21.43 64.13 21.46 1.33 1.35 22.33 22.33 17.73 393.1 21.66 1.13 1.23 1.33 22.33 17.73 393.1 21.66 1.14 1.23 1.23 22.33 17.74 23.33 11.06 11.11 27.33 12.33 22.33 17.74 23.33 11.06 11.33 12.33 12.33 22.33 17.74 23.33 11.06 11.11 27.33 12.33 22.34 17.74 23.33 11.11	1764	508.5	616.5	21.53	1.88	1.42	1829	405.4	272.2	22.20	1.35	0.49
[176 2446 266.0 2154 1.00 1.41 1831 185 678.2 22.21 1778 4169 460.0 2155 1.40 1.41 1137 20.23 22.23 22.24 22.23 22.24	1765	464.9	360.5	21.53	111	0.81	1830	260.0	941.9	22.20	1.51	0.97
1707 592.0 965.0 71.5 17.7 <	1766	244.6	286.0	21.54	1.40	1.41	1831	18.8	678.2	22.21	1.07	0.83
1708 416.9 446.9 21.56 1.78 1.51 1833 611.7 572.3 22.34 1770 214.4 549.1 21.56 2.46 11.3 572.3 22.35 1770 214.4 549.1 21.65 21.69 11.3 572.4 22.34 1770 214.3 51.61 1.11 0.73 1887 156.4 22.32 1776 256.6 21.62 1.01 1.39 18.37 22.32 1776 256.6 21.62 1.03 1.34 1.22 22.34 1776 256.6 21.62 1.03 1.33 22.32 22.32 1776 256.6 21.62 1.03 0.73 1.84 22.32 1778 353.5 21.67 1.14 1.17 22.32 22.32 1783 353.5 21.67 1.13 1.14 1.17 22.32 1783 353.5 21.67 1.14 1.12 23.34 </td <td>1767</td> <td>592.0</td> <td>965.0</td> <td>21.55</td> <td>1.72</td> <td>1.70</td> <td>1832</td> <td>51.9</td> <td>648.9</td> <td>22.22</td> <td>1.47</td> <td>1.12</td>	1767	592.0	965.0	21.55	1.72	1.70	1832	51.9	648.9	22.22	1.47	1.12
1770 214.3 559.9 21.66 1.48 1.37 183.4 611.6 567.2 22.25 1777 307.3 928.2 21.16 1.21 12.00 32.34 71.47 37.45 51.6 50.6 50.5 25.45 71.47 25.25 71.47 72.25	1768	416.9	446.9	21.55	1.78	1.51	1833	611.3	522.8	22.24	1.36	0.71
1770 214.3 6461 21.56 2.40 1.18 818.3 56.3 22.25 1777 389.1 271.3 21.57 21.67 1.01 18.87 16.65 22.35 1773 389.1 271.3 21.67 1.01 18.87 15.65 22.25 1775 380.1 271.3 21.67 1.41 1.22 18.87 15.65 22.25 1775 380.1 21.67 1.46 1.23 18.47 22.30 1776 383.1 21.62 1.00 13.81 12.75 95.44 22.23 1776 383.1 21.67 1.14 1.23 18.41 22.35 1778 383.1 21.67 1.13 1.17 1.25 96.47 22.23 1781 383.1 21.67 1.13 1.17 1.26 1.23 22.35 1782 383.1 21.67 1.13 1.17 1.29 23.35 24.4 22.35	1769	214.2	539.9	21.56	1.48	1.37	1834	611.7	637.2	22.25	1.70	1.24
1177 307.3 238.3 2167 1.47 1.40 1.88 538.4 536.3 514.7 22.53 1777 2110 07.3 2110 1.47 1.43 1.23 1.88 536.5 714.7 256.5 74.4 22.33 1777 256.5 566.5 21.61 1.11 0.73 184.0 57.4 22.33 1777 256.5 566.3 21.62 1.14 0.73 184.1 27.5 66.2 22.33 1778 555.0 667.4 21.63 1.13 0.73 184.1 23.33 22.33 178 353.0 21.65 1.14 0.73 184.1 23.33 22.33 22.33 178 233.0 1.44 1.14 1.16 1.14 1.14 1.14 22.33 22.33 22.33 22.34 24.4 22.33 22.34 24.4 22.33 22.36 22.33 22.36 22.33 22.36 22.36 22.36	1770	214.3	649.1	21.56	2.40	1.18	1835	616.6	300.9	22.26	1.21	0.48
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1771	307.3	928.2	21.57	1.37	1.20	1836	353.7	226.5	22.28	1.04	1.64
Intrastructure January	1772	389.1	271.3	21.59	1.49	1.01	1837	162.5	564.3	22.29	1.24	1.61
IIII Job <td>1774</td> <td>131.0</td> <td>898.3 F 1 F 7</td> <td>21.59</td> <td>1.34</td> <td>1.22</td> <td>1636</td> <td>0.952</td> <td>1.14.1</td> <td>00.22</td> <td>#6:0 •</td> <td>1.10</td>	1774	131.0	898.3 F 1 F 7	21.59	1.34	1.22	1636	0.952	1.14.1	00.22	#6:0 •	1.10
ITT TAT <td>1776</td> <td>1.061</td> <td>1.010</td> <td>71.60</td> <td>45.1 1.139</td> <td>1.30</td> <td>16251</td> <td>020.4</td> <td>0.027</td> <td>10.22</td> <td>1.1</td> <td>1.25</td>	1776	1.061	1.010	71.60	45.1 1.139	1.30	16251	020.4	0.027	10.22	1.1	1.25
ITT 45.8 238.2 21.0 0.0	1776	4.7.K	0.000	10.12	11.1	0.73	1641	001.0	1.11	10.11	1 52	1.35
ITT SS5.0 419.7 210.2 110 223.1 113.7 216.5 113 223.15 212.1 223.2 223.	1777	476.8	1.000	20.12	9 	1.35	1201	0.14	1.450	22.23	2.32	0.22
ITT 333.1 313.7 2163 113 0.70 1844 333.6 212.1 22.50 ITT8 33.0 667.4 216.5 113 0.70 1844 33.6 22.50 ITT8 39.0 677.4 216.5 113 10.6 1846 29.3 396.1 22.50 ITT8 39.0 178.3 201.7 143.2 2167 1.44 116 1846 29.3 396.1 22.50 ITT85 200.3 391.1 143.7 1.16 1184 33.6 22.50 IT785 200.3 164.7 1.43 1.16 1186 28.4 72.5 1790 187.4 21.70 1.29 1.41 1.97 18.5 23.01 23.01 1790 187.4 21.77 1.41 1.96 188.7 27.23 23.01 1791 187.4 21.77 1.41 1.96 188.6 37.8.1 23.05 24.64	1778	2020	410.7	1 63	8	100	5707 1843	196.2	3 7 0 K	22.38		1.16
1780 330 6674 2163 121 0.03 1845 573.5 366.7 22.5 1781 82.2 960.3 21.65 113 105 1847 25.3 847.1 22.5 1783 361.7 143.2 361.7 143.2 105 1847 25.3 847.1 22.5 1786 450.7 143.7 11.64 11.3 11.7 1441 26.3 847.1 22.65 1786 457.7 15.4 11.67 11.3 11.7 1855 65.3 23.65 1786 457.7 166 1.41 11.97 1855 15.2 23.25 1791 372.9 857.1 177 1855 132.7 363.1 23.26 1791 372.9 857.1 11.97 11.87 11.87 132.3 893.1 22.65 1793 181.9 71.1 11.8 11.66 11.81 11.85 23.2.65 1793	1779	353.5	313.7	21 62	113	12.0	1844	383.6	212.1	22.39	1.39	1.36
1781 82.2 960.3 2165 110 0.00 1846 29.3 847.1 22.55 1784 601.7 142.2 21.66 11.5 0.78 1844 24.13 28.73 23.13 27.55 1784 601.7 142.2 21.66 11.5 11.67 138.7 24.61 23.3 847.1 27.53 1785 280.3 11.67 11.81 11.66 11.81 11.66 23.3 847.1 22.63 1786 183.4 14.71 11.81 11.66 11.81 11.66 23.3 847.1 22.63 1786 183.4 14.71 14.8 14.66 185.7 33.01 23.65 23.06 23.64 27.53 23.01 1790 57.10 12.47 14.16 186 186.7 33.72 23.01 23.26 23.06 23.64 27.53 23.01 23.66 23.64 27.53 23.01 23.76 23.66 23.66 2	1780	93.0	697.4	21.63	1.21	0.93	1845	573.5	396.2	22.50	1.22	1.14
1782 203.9 331.2 21.66 11.5 0.78 1847 24.1.2 22.57 1784 601.7 14.79 12.85 1.66 11.3 11.7 24.1.2 22.64 1785 500.7 14.73 11.67 11.8 11.6 11.85 260.3 21.67 12.4 12.66 13.3 12.67 12.64 17.1 24.1 22.69 1785 530.1 54.7 14.3 11.3 11.7 1851 56.1 32.61 22.99 1789 537.1 44.3 1.73 14.66 185.6 56.3 32.1 22.99 1799 1779 18.61 17.7 14.1 14.1 14.7 12.52 23.03 1791 133.3 25.1 14.1 14.7 136.7 13.6 23.2.3 23.03 1792 180 75.1 14.1 14.7 136.7 33.01 26.6 23.2.3 24.66 23.2.3 23.03 <t< td=""><td>1781</td><td>82.2</td><td>960.3</td><td>21.63</td><td>101</td><td>0.20</td><td>1846</td><td>29.3</td><td>847.1</td><td>22.53</td><td>1.61</td><td>0.98</td></t<>	1781	82.2	960.3	21.63	101	0.20	1846	29.3	847.1	22.53	1.61	0.98
1783 361.2 579.6 21.66 1.33 1.05 184.8 255.3 663.8 22.57 1786 477.4 142.2 21.67 1.44 1.46 185.1 270.3 93.1 236.5 12.7 12.4 12.6 12.4 12.6	1782	203.9	391.2	21.66	1.15	0.78	1847	241.2	231.2	22.55	1.72	1.04
1784 601.7 14.2 21.67 12.4 12.9 184.9 466.1 33.8.7 23.5.6 13.2.6 13.8.7 23.5.6 13.2.6 13.8.7 23.5.6 13.2.6 13.8.7 23.5.6 13.2.6 13.8.7 23.5.6 13.2.6 13.6.1 13.6.1 13.6.7 23.5.6 13.2.8 14.1 13.6 13.6.1 23.5.6 13.7.2 21.6.7 13.8.7 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 23.5.6 <td< td=""><td>1783</td><td>361.2</td><td>579.6</td><td>21.66</td><td>1.33</td><td>1.05</td><td>1848</td><td>255.3</td><td>663.8</td><td>22.57</td><td>1.36</td><td>0.85</td></td<>	1783	361.2	579.6	21.66	1.33	1.05	1848	255.3	663.8	22.57	1.36	0.85
1785 296.3 21.67 164 11.6 1851 286.4 47.1 22.64 1787 236.4 874.0 21.67 1.43 1.11 1851 22.65 47.1 22.64 1787 236.4 874.0 21.67 1.43 1.43 71.88 1.33 1.01 73.55 53.7 37.2 39.1 22.64 1788 339.1 43.7 1.08 1.16 1.85 53.7 37.2 32.0 1791 31.2.3 855.3 21.70 1.21 1.41 1.66 1856 53.7 37.2 33.01 23.30 23	1784	601.7	142.2	21.67	1.24	1.29	1849	466.1	328.7	22.63	2.00	0.86
1786 457.4 874.0 21.67 11.3 11.7 11.85 12.05 12	1785	269.2	296.3	21.67	1.64	1.16	1850	288.6	447.1	22.64	0.43	-0.89
1787 238.6 18.3 11.67 14.43 14.41 14.53 15.55 55.23 75.15 23.07 1780 55.47 16.37 11.66 11.34 11.66 11.34 11.67 23.05 55.3.1 75.15 23.07 1790 57.71 16.77 11.66 11.77 11.66 11.85 55.3.3 30.05 23.3.01 1792 178.3 94.05 21.77 11.41 11.76 1185 55.3.3 23.05 1792 178.3 312.9 73.14 11.42 11.66 1185 23.3.7 1795 77.1 11.18 11.68 11.68 11.68 23.7.6 23.0.7 1796 64.1 41.4 11.76 11.68 11.66 23.7.6 24.66 1797 64.1 41.4 11.76 10.65 11.66 26.6 23.6.4 24.66 1798 64.1 11.6 11.66 11.66 11.66 26.6	1786	457.4	874.0	21.67	1.13	1.17	1851	270.3	893.1	22.66	1.44	0.86
1788 359.1 443.7 71.68 1.24 1.60 1854 12.23 934.7 22.93 1790 57.70 182.4 21.70 1.27 1.41 1.97 1855 553.7 37.2 393.7 32.33 177 1791 31.23 365.3 21.70 1.27 1.41 1.97 1855 553.7 37.2 33.01 73.3 30.35 32.30 173.2 23.30 173.2 23.30 173.2 23.30 173.2 23.30 173.2 23.30 173.2 23.30 173.2 23.30 173.2 23.30 143.5 13.30 13.35 23.35 23.36 23.31 73.1 23.3 23.06 23.33 13.05 23.36	1787	238.6	152.8	21.67	1.43	1.41	1852	510.8	785.5	22.97	1.45	1.04
1790 5770 1771 1195 5770 1271 1195 5770 1271 1271 1271 1271 1271 1271 1271 1271 1271 1273 <th< td=""><td>1788</td><td>339.1</td><td>443.7</td><td>21.68</td><td>1.24</td><td>1.60</td><td>1853</td><td>102.8</td><td>984.7</td><td>22.99</td><td>1.57</td><td>0.73</td></th<>	1788	339.1	443.7	21.68	1.24	1.60	1853	102.8	984.7	22.99	1.57	0.73
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1789	454.7	167.2	21.69	1.41	1.97	1854	122.3	800.3	23.00	1.14	0.88
1791 1333 950.3 1.10 1.05 <th1.05< th=""> 1.05 1.05 <th< td=""><td>1421</td><td>0.726</td><td>182.4</td><td>21.70</td><td>1.27</td><td>1.41</td><td>1855</td><td>553.7</td><td>37.2</td><td>23.07</td><td>0.7</td><td></td></th<></th1.05<>	1421	0.726	182.4	21.70	1.27	1.41	1855	553.7	37.2	23.07	0.7	
1793 181.9 731.6 11.1 11.8 1.00 11.8 1.00 11.8 1.00 11.8 1.00 11.7 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4 <	1611	6.210	040.0	21.72	60.T	0.65	1650	132.4	9,000	67.07 53 33	0.55	90.0-
1794 222.2 234.6 21.7 1.43 1.76 23.6 24.6 24.6 1795 87.2 300.7 21.77 1.49 1.00 1660 335.8 733.4 24.60 1795 614.1 41.4 21.77 1.49 2.04 1660 335.8 733.4 24.56 1798 44.45 27.78 1.04 0.47 1.30 1861 379.7 342.9 24.84 1798 44.16 27.78 1.16 0.47 1.22 1.30 1861 379.7 342.9 24.84 1790 160.6 234.2 21.79 1.16 0.47 1.22 1.30 1.36 2.46 1.45	1793	181.9	751 A	12.17	118	1.68	1858	100.1	861.2	23.65	0.31	-0.63
1795 77.2 300.7 21.77 1.09 -0.10 1660 375.4 24.64 1796 64.1 77.3 30.7 21.77 1.09 -0.10 1660 375.4 24.64 1796 64.1 77.4 1.42 1.30 1660 375.4 24.64 1798 444.0 78.8 21.76 1.04 0.47 342.9 24.64 1800 213.3 519.2 21.87 1.16 1.24 342.9 24.64 1801 213.3 519.2 21.87 1.16 1.24 379.7 342.9 24.64 1801 213.5 515.6 21.48 1.16 1.24 1.25 1.29 1.46 1802 550.1 21.90 1.46 1.47 1.82 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46 1.46	1794	222.2	254.8	21 73	1.10	1 78	1850	6315	923.6	24.05	1.07	-0.31
1796 88.2 337.5 21.74 1.42 1.30 1861 379.7 342.9 24.84 1797 61.41 41.41 21.75 1.49 2.04 1861 379.7 342.9 24.84 1797 61.41 41.41 21.75 1.49 2.04 1861 379.7 342.9 24.84 1799 41.15 41.61 7.17 11.16 11.14 1.25 1.14 1.25 1.49 2.04 1861 379.7 342.9 24.84 1801 216.5 51.45 21.78 1.16 1.14 1.22 1802 536.1 61.56 21.83 2.98 0.47 1.42 1.26 1802 536.1 51.66 1.16 1.16 1.12 1.26 1806 506.5 51.1 21.99 1.86 1.86 1.86 1806 535.3 61.3 21.93 1.36 1.86 1.86 1.86 1.86	1795	27.2	300.7	21.72	1.09	-0.10	1860	325.8	753.4	24.56	-0.41	-0.21
1787 614.1 41.4 21.75 1.49 2.04 1798 44.14 27.75 1.04 0.47 1799 41.15 27.83 21.76 1.04 0.47 1799 41.15 27.83 21.76 1.04 0.47 1800 180.6 24.4 21.77 1.14 1.22 1800 231.3 519.0 21.87 1.13 0.47 1803 254.3 719.0 21.87 1.75 1.22 1803 256.1 61.66 21.87 1.56 1.24 1806 206.5 577.1 21.90 1.56 1.54 1806 205.5 577.1 21.90 1.56 1.54 1806 205.5 571.2 21.90 1.54 1.82 1806 528.4 907.5 21.92 1.88 -0.04 1807 238.4 746.0 21.92 1.40 1.53 1808 528.4	1796	89.2	327.5	21.74	1.42	1.30	1861	379.7	342.9	24.84	-0.18	-0.71
1798 444.0 278.8 21.76 104 0.47 1800 491.5 549.2 21.78 110 0.62 1800 531.6 549.2 21.78 111 0.65 1801 213.3 519.2 21.87 1.78 1.11 0.65 1801 213.5 51.6 51.6 21.87 1.78 1.27 1802 254.3 71.90 21.87 1.78 1.28 1.28 1803 256.1 61.6 21.87 1.78 1.26 1.28 1806 206.9 557.1 21.90 1.41 1.82 1806 206.5 557.1 21.90 1.46 1.66 1807 332.4 760.0 1.24 1.82 1.03 1806 206.5 557.1 21.92 1.48 0.02 1807 332.4 776.0 21.93 1.83 0.03 1811 207.5 21.97 0.84 0.0	1797	614.1	41.4	21.75	1.49	2.04						
18799 411.5 456.2 21.78 11.0 0.62 18001 213.3 519.2 21.179 11.4 11.4 18012 531.3 519.2 21.187 11.6 11.4 18012 531.3 519.3 21.83 2.98 0.47 1802 536.1 615.6 21.83 2.98 0.47 1803 556.1 51.90 21.83 1.95 1.42 1806 566.0 304.0 21.90 1.41 1.22 1806 532.4 766.0 21.90 1.41 1.82 1806 532.4 907.5 21.92 1.40 1.83 1808 532.4 907.5 21.93 1.36 1.84 1809 528.4 907.5 21.93 1.36 1.46 1811 66.4 787.0 21.94 0.21 1.88 1812 66.4 787.0 21.94 0.21 1.88 1815	1798	444.0	278.8	21.76	1.04	0.47						
1800 183.5 254.3 21.79 11.4 1800 531.6 615.6 21.87 11.4 1.22 1802 531.6 615.6 21.87 1.79 1.42 1803 545.1 71.90 1.42 1.42 1806 566.0 304.0 21.87 1.55 1.29 1806 566.1 304.0 21.88 1.35 1.03 1806 566.1 304.0 21.88 1.35 1.03 1806 335.4 667.1 21.90 1.56 1.54 1807 335.3 613.2 21.92 0.88 -0.04 1808 335.3 613.2 21.93 0.92 1.88 1811 202.9 57.8 21.94 1.58 1.68 1811 202.9 57.8 21.97 0.38 0.01 1812 66.7 21.97 0.38 0.36 1.37 1.68 1811 202.9 57	1799	411.5	469.2	21.78	1.10	0.62						
1800 131.5 51.9.5 21.82 1.14 1.22 1800 359.1 61.6 21.87 1.79 1.47 1800 359.1 61.6 21.87 1.79 1.42 1805 356.1 61.6 21.87 1.79 1.42 1806 356.1 61.6 21.87 1.55 1.39 1806 206.5 557.1 21.90 1.56 1.54 1806 238.4 76.0 21.90 1.41 1.82 1806 338.4 76.0 21.92 1.40 1.53 1809 538.7 775.2 21.92 1.40 1.53 1811 205.5 21.92 1.40 1.53 1.68 1811 61.79 235.4 21.96 0.58 0.04 1815 537.3 21.97 0.88 0.19 1.168 1815 537.3 27.01 1.35 0.24 1.86 1816 67.1 </td <td>1800</td> <td>169.6</td> <td>254.2</td> <td>21.79</td> <td>1.15</td> <td>1.14</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	1800	169.6	254.2	21.79	1.15	1.14						
1803 254.3 713.0 2.4.5 1.4.5 <th1< td=""><td>1001</td><td>£21 6</td><td>212.2</td><td>79.17</td><td>1.14</td><td>1.22</td><td></td><td></td><td></td><td></td><td></td><td></td></th1<>	1001	£21 6	212.2	79.17	1.14	1.22						
1004 359.1 615.6 21.87 1.55 1.93 1805 566.0 394.0 21.88 1.35 1.03 1806 308.4 76/0.0 21.90 1.45 1.54 1807 308.4 76/0.0 21.90 1.45 1.54 1807 335.3 61.3.2 211.92 0.88 -0.04 1808 335.3 61.3.2 211.92 0.88 -0.04 1809 528.4 907.5 211.94 1.53 1.80 1811 202.9 578.8 211.94 1.21 1.58 1811 202.9 578.8 211.94 1.21 1.58 1811 202.9 576.8 21.97 0.38 0.04 1815 232.4 21.96 0.36 0.19 1.68 1816 547.8 700.5 21.97 1.38 1.08 1816 547.8 700.5 21.99 1.77 0.99 1816	1803	254.3	0.017	21.87	1 70							
1805 566.0 304.0 21.88 1.35 1.03 1807 353.3 613.2 21.90 1.54 1.54 1807 353.3 613.2 21.90 1.54 1.82 1807 353.3 613.2 21.90 1.56 1.54 1807 353.3 613.2 21.92 0.88 -0.04 1810 185.7 75.6 21.92 1.40 1.53 1811 202.9 578.8 21.94 1.21 1.56 1811 202.9 578.8 21.94 1.21 1.58 1812 66.4 7.70 21.95 0.36 0.24 1812 617.9 235.4 21.97 0.38 0.19 1815 547.8 70.5 21.97 0.38 0.10 1815 547.8 70.5 21.97 0.38 0.19 1816 547.8 70.5 21.97 0.38 0.21 1816 547.	1804	359.1	615.6	21.87	1.55	1.29						
1806 206.3 557.1 21.90 1.56 1.54 1807 338.4 746.0 21.90 1.41 1.82 1808 532.3 61.3 21.29 1.41 1.82 1808 532.3 61.3 21.29 1.40 1.53 1809 538.7 756.2 21.92 1.40 1.53 1810 188.7 756.2 21.93 1.39 0.92 1811 66.1 776.2 21.95 0.84 0.24 1812 66.1 776.2 21.95 0.84 0.24 1815 61.79 236.4 21.96 0.56 0.44 1815 637.8 71.97 0.88 0.19 1.17 1816 677.9 27.01 1.35 1.66 1.35 1.68 1817 269.9 309.6 21.97 0.88 0.19 1.77 0.20 1816 637.3 70.3 1.37 1.68 1.37	1805	566.0	304.0	21.88	1.35	1.03						
1800 338.4 746.0 141 1.82 1800 332.3 6.10 1.43 -0.04 1800 538.4 907.5 21.92 0.88 -0.04 1800 538.4 907.5 21.93 1.40 1.53 1811 265.4 775.2 21.93 1.39 0.92 1811 203.5 778.2 21.93 1.31 1.58 1811 205.5 71.95 0.84 0.24 1815 232.9 270.5 21.97 0.88 0.19 1815 232.9 270.5 21.97 0.88 0.19 1815 232.9 270.5 21.97 0.88 0.19 1817 565.3 20.01 2.17 0.03 1.168 1817 565.3 20.01 2.13 0.13 1.168 1817 565.3 22.01 1.37 1.68 1.38 1818 363.5 565.3 22.01	1806	206.9	557.1	21.90	1.56	1.54						
B009 528.4 91.4.2 104 1800 158.7 725.2 21.93 1.30 1811 202.9 578.8 21.94 1.53 1811 205.4 725.2 21.93 1.30 0.92 1811 205.4 725.2 21.94 1.21 1.58 1813 421.1 235.4 21.96 0.34 0.24 1814 61.79 235.4 21.96 0.36 0.44 1815 21.97 0.38 0.19 1.18 1.85 1815 235.4 21.96 0.36 0.44 1.81 1816 54.78 70.15 21.97 1.38 1.21 1817 269.9 209.6 21.99 1.77 0.99 1818 36.5.3 22.01 1.34 1.68 1.43 1819 46.1 1.37 1.06 0.41 1.81 1820 339.1 115.7 2.09 0.41 1	1807	338.4	746.0	21.90	1.41	1.82						
1810 185.7 75.9 1.31 1.58 1.61 1.21 1.58 1.61 <th1.61< th=""> 1.61 1.61 <th< td=""><td>1800</td><td>502.3</td><td>013.2 007 K</td><td>26.12</td><td>0.88</td><td>-0.04</td><td></td><td></td><td></td><td></td><td></td><td></td></th<></th1.61<>	1800	502.3	013.2 007 K	26.12	0.88	-0.04						
1811 202.9 578.8 21.94 1.21 1.58 1813 66.4 787.0 21.95 0.84 0.24 1813 617.9 235.4 21.95 0.84 0.24 1815 617.9 235.4 21.95 0.86 0.44 1815 232.4 21.96 0.36 0.19 1.16 1815 235.4 21.97 0.38 0.19 1.17 1816 547.8 70.5 21.97 1.35 1.21 1817 269.9 309.6 21.97 1.35 1.21 1817 269.9 309.6 21.97 1.37 1.68 1818 303.5.3 22.01 1.37 1.68 1.43 1819 40.1 13.5 2.2.07 1.34 1.60 1820 339.1 115.7 2.34 1.50 1.43	1810	185.7	725.2	21.93	1.39	0.92						
1812 66.4 787.0 21.95 0.84 0.24 1813 421.1 235.3 21.95 1.58 1.68 1815 537.8 70.5 21.97 0.88 0.44 1815 537.8 70.15 1.197 1.36 1.21 1815 537.8 70.15 21.97 0.88 0.19 1817 569.9 309.6 2.197 0.88 0.19 1817 569.9 309.6 2.1.97 0.88 0.19 1817 569.9 309.6 2.2.01 1.37 1.68 1818 303.5 96.3 32.01 1.37 1.68 1819 40.1 1.37 1.68 0.43 1820 339.1 115.7 2.2.07 1.34 1.50	1811	202.9	578.8	21.94	1.21	1.58						
1813 421.1 235.3 21.95 1.58 1.68 1814 617-9 235.4 21.96 0.36 0.44 1815 547.8 790.1 21.97 0.38 0.19 1817 269.9 309.6 21.99 1.77 0.99 1818 363.5 965.3 22.01 1.77 0.99 1819 40.1 133 22.07 1.34 1.50	1812	66.4	787.0	21.95	0.84	0.24						
1815 517.9 235.4 21.96 0.36 0.44 1815 547.8 790.5 21.97 0.38 0.19 1817 269.9 309.6 21.99 1.77 0.99 1818 365.3 965.3 22.01 1.37 1.68 1819 40.1 133 22.00 1.37 1.68 1820 339.1 115.7 22.07 1.34 1.50	1813	421.1	235.3	21.95	1.58	1.68						
1816 5478 704.0 21.97 1.38 0.19 1817 269.9 309.6 21.99 1.77 1.35 1.21 1818 363.5 965.3 22.01 1.37 1.68 1819 40.1 133 22.07 1.37 1.68 1819 339.1 115.7 22.07 1.34 1.50	1015	917.9	235.4	21.96	0.36	0.44						
1817 269.9 309.6 21.99 1.77 0.99 1818 303.5 965.3 22.01 137 1.68 1819 40.1 135.2 22.07 0.73 0.43 1820 339.1 115.7 22.07 1.34 1.50	1816	547.8	2.012	26.12	0.88	6T-0						
1818 363.5 965.3 22.01 1.37 1.68 1819 40.1 193.3 22.06 0.79 0.43 1820 339.1 115.7 22.07 1.34 1.50	1817	269.9	309.6	21.99	1.77	0.99						
1819 40.1 193.3 22.06 0.79 0.43 1820 339.1 115.7 22.07 1.34 1.50	1818	363.5	965.3	22.01	1.37	1.68						
1000 1001 1101 7210 1134 1100	1819	40.1	193.3	22.06	0.79	0.43						
	1040	1.800	110.1	22.01	1.34	T.5U						



FIG. 1. The color-magnitude diagram obtained for M71. The photometry is listed in Table 2. Stars listed in Arp and Hartwick's Table 1 in the vicinity of the giant branch are shown as open triangles. Variables are shown as open circles and are labeled (see text). The fiducial derived from this diagram is shown as the solid line. Reddening corrections have not been applied to the data in this diagram.

& Hartwick's (1971) Fig. 3 and Table 2(a) we find a similar result of $V_{\rm HB} = 14.44 \pm 0.08$. For comparison purposes the stars measured photoelectrically by Arp and Hartwick and listed in their Table 1 that lie in the red giant branch region are plotted as open triangles in Fig. 1. The variable star candidates discussed in Sec. 4 are plotted as open circles. The solid curve is the adopted fiducial, which was drawn by hand through the highest density of points and is in reasonable agreement with Arp and Hartwick's fiducial—though it should be pointed out that their photoelectric study is not necessarily complete. Unfortunately, Cudworth's magnitude limit is approximately 1 mag brighter than the turn-up point of the subgiant branch and the location of this point is critical for most age determination methods, as will be seen in Sec. 3.2 (see also VandenBerg *et al.* 1990).

Figure 2 is a finding chart for the stars in Table 2 and was produced using that data. The completeness of this map is thus dependent on the ability of DAOPHOT to find faint stars and accurately measure their magnitudes. Comparison of Fig. 2 with Richer & Fahlman's (1988) Fig. 1 shows a very good agreement.

Our estimate of the M71 fiducial is tabulated in Table 3, columns (1) and (2). Table 2 does not include errors in the magnitudes and colors of the stars—we include in columns (3) and (4) of Table 3 typical error values in each magnitude bin, and the corresponding error in B - V color at that point. These values are the median errors in V and B - V for

the stars contained in the bin whose center lies at the appropriate entry in the table.

3.2 Comparison with 47 Tucana

VandenBerg *et al.* (1990) have recently demonstrated the effectiveness of a new method of relative age determinations. Their procedure involves shifting fiducials of two clusters so that the colors of the turn off points, and the magnitudes at points on the main sequence $0^{m}05$ redder than the turnoff colors, are matched together. If the two clusters are of similar metallicity then any difference in the color of the giant branches can be interpreted as an age difference. Sarajedini & Demarque (1990) have proposed a similar scheme in which the difference in color between the turnoff and the base of the subgiant region is used to estimate ages, allowing age differences to be computed fairly easily.

47 Tuc is a globular cluster similar in many respects to M71. Hesser *et al.* (1987, hereafter referred to as H87) adopt a metallicity for 47 Tuc of -0.65, and discuss the reasoning behind this choice. Metallicity (defined here to mean [Fe/H]) estimates for M71 range from -0.4 (Bessell 1983) to -1.2 (Cohen 1980, using echelle spectra). Leep *et al.* (1987) restrict the value to between -0.6 and -1.0. As shall be seen below, theoretical isochrones computed for an [Fe/H] = -0.78 provide a good fit to our M71 fiducial,



FIG. 2. Identification chart for the large field photometry. This map was constructed using the photometry list given in Table 2, and is therefore not guaranteed to be complete. The field used to search for variables is the area enclosed by the solid lines in the southwest portion of the figure. The variables themselves (discussed in Sec. 4 of the text) are marked as open circles. The plate scale is 0."21 per pixel.

though the [Fe/H] = -0.65 isochrones also fit relatively well.

Following the VandenBerg et al. technique [and noting the caveats for this procedure mentioned there and in VandenBerg & Stetson (1991)] we have performed a comparison between 47 Tuc and M71 which is shown in Fig. 3. The 47 Tuc fiducial is the published fiducial of H87, shifted by +0.379 in V and +0.235 in B - V. These shifts are very close to the difference in distance moduli $[(M-m)_{M71} - (M-m)_{47 \text{ Tuc}} = 0.4]$ and reddening $[E(B-V)_{M71} - E(B-V)_{47 \text{ Tuc}} = 0.24]$ for the two clusters, using the results published by Richer & Fahlman (1988) and H87. The agreement between the two fiducials is readily apparent. The small difference between the giant branches from 14 < V < 16 may be due merely to our estimate of the poorly defined M71 fiducial; indeed, the 47 Tuc fiducial does not seem out of place when plotted on the M71 color-magnitude diagram. Arp & Hartwick (1971) sketched a very similar fiducial-in their Fig. 3 the turnoff color is at B - V = 0.76 and the base of the giant branch is at

TABLE 3. M71 fiducial sequence.

V	B-V	ϵ_V	ϵ_{B-V}
12.50	1.72	0.04	0.06
13.00	1.55	0.04	0.07
13.50	1.42	0.04	0.06
14.00	1.305	0.04	0.06
14.50	1.21	0.04	0.06
15.00	1.15	0.04	0.06
15.50	1.10	0.04	0.06
16.00	1.075	0.04	0.06
16.50	1.06	0.04	0.06
17.00	1.04	0.04	0.06
17.20	1.02	0.04	0.06
17.40	0.99	0.04	0.06
17.50	0.96	_	—
17.57	0.93		—
17.58	0.92		
17.60	0.875	0.01	0.01
17.63	0.835	_	
17.73	0.795	0.03	0.04
17.80	0.785	0.01	0.01
17.90	0.777	0.01	0.01
18.00	0.775	0.01	0.02
18.20	0.78	0.01	0.01
18.40	0.793	0.01	0.01
18.60	0.815	0.01	0.01
18.80	0.836	0.01	0.01
19.00	0.86	0.01	0.01
19.20	0.885	0.01	0.02
19.40	0.915	0.01	0.01
19.60	0.945	0.01	0.02
19.80	0.98	0.01	0.01
20.00	1.015	0.01	0.02
20.20	1.055	0.01	0.02
20.40	1.095	0.01	0.02
21.00	1.25	0.02	0.03

dence for a substantial age difference between M71 and 47 Tuc. This conclusion is contrary to the result reported by Heasley & Christian (1991), that M71 is ~ 3 Gyr older than 47 Tuc. However, it must be stressed that our conclusion depends critically on the fiducial location at and just above the base of the red giant branch. It is clear from Fig. 1 that our fiducial is not well defined in that region. Consequently we cannot firmly exclude the possibility of a relative age difference between 47 Tuc and M71. Figure 4 compares M71 with oxygen enhanced theoretical isochrones computed by Berchusch & VandenBerg (1901)

B - V = 1.00. This agrees very well with the fiducial presented here. We do not, therefore, find any convincing evi-

In both (a) and (b) the isochrones have been shifted using a distance modulus of 13.7 and a reddening of 0.28. An additional shift in B - V of 0.015 was required to match the fiducial with the isochrones. Figure 4(a) compares the fiducial to the isochrones. Below the turnoff the agreement between observation and theory is good, but at the turnoff the fiducial crosses between the 14 and 16 Gyr isochrones. This mismatch, together with that evident along the giant branch is, at least in part, due to the difficulty of defining the fiducials with sparse and scattered data. In Fig. 4(b) we plot the isochrones over the individual points in the color-magnitude diagram defined by our photometry. It can be seen that

HJDa	Filter	H1	H2	H3	H4	HJDa	Filter	H1	H2	H3	H4
(2446200.0+)						(2446200.0+)					
(1)	(2)	(3)	(4)	(5)	(6)	(1)	(2)	(3)	(4)	(5)	(6)
58.86377	v	16.237	19.522	18.866	17.607	59.89504	В	16.828	19.853	20.032	18.348
58.86768	v	16.247	19.474	18.878	17.617	59.90285	В	16.821	19.801	20.054	18.333
58.87158	v	16.257	19.458	18.886	17.620	59.91067	В	16.804	19.757	20.021	18.342
58.87549	v	16.269	19.437	18.904	17.631	59.91848	В	16.807	19.746	20.002	18.355
58.87939	v	16.287	19.414	18.925	17.637	59.92629	В	16.839	19.787	19.993	18.381
58.88330	v	16.289	19.394	18.943	17.659	59.93410	В	17.137	19.853	19.964	18.394
58.88721	v	16.293	19.446	18.966	17.664	59.94582	В	16.844	19.835	19.946	18.404
58.89502	v	16.284	19.379	18.998	17.673	60.08645	v	16.309	_		17.843
58.89893	v	16.273	19.396	19.028	17.672	60.09036	v	16.303		18.782	17.782
58.90283	v	16.221	19.447	19.049	17.670	61.04350	В	16.811	19.846	19.979	18.324
58.90674	v	16.205	19.468	19.051	17.669	61.05132	В	16.770	19.780	19.927	18.313
58.91064	v	16.198	19.502	19.045	17.676	61.05913	в	16.786	19.778	19.950	18.318
58.91455	v	16.218	19.487	19.029	17.665	61.06694	в	16.804	19.771	19.923	18.309
58.91846	v	16.238	19.523	18.999	17.666	61.93024	v	16.282	19.465	18.914	17.795
58.92236	v	16.261	19.493	18.967	17.648	61.93805	v	16.299	19.499	18.891	17.921
58.92627	v	16.299	19.481	18.928	17.634	61.94196	v	16.303	19.514	18.881	18.012
58.93408	v	16.233	19.397	18.864	17.592	61.94587	v	16.299	19.521	18.888	18.113
58.95361	v	16.209	19.403	18.869	17.582	61.95368	v	16.269	19.488	18.874	18.233
58.95752	v	16.187	19.447	18.868	17.575	61.95758	v	16.222	19.465	18.859	18.270
58.96143	v	16.200	19.433	18.865	17.581	61.96149	v	16.197	19.417	18.853	18.292
58.96533	v	16.200	19.499	18.851	17.583	61.96540	v	16.183	19.407	18.837	18.289
58.97314	v	16.234	19.488	18.864	17.582	61.96930	v	16.173	19.367	18.860	18.237
58.97705	v	16.248	19.491	18.842	17.576	61.97321	v	16.218	19.392	18.826	18.267
59.03174	в	16.830	19.831	19.946	18.281	61.97712	v	16.248	19.382	18.825	18.201
59.04346	в	16.822	19.878	19.937	18.309	61.98103	v	16.286	19.406	18.830	18.076
59.05127	В	16.869	19.636	19.975	18.311	61.98884	v	16.303	19.414	18.823	17.986
59.05909	в	16.819	19.791	20.022	18.279	61.99274	v	16.317	19.451	18.840	17.914
59.06690	в	16.882	19.757	19.985	18.389	61.99665	v	16.308	19.464	18.818	17.842
59.08643	в	16.845	19.784	20.218	18.308	62.02399	B	16.710	19.697	20.076	18.082
59.09424	в	16.815	19.800	20.267	18.297	62.03181	в	16.815	19.736	19.996	18.308
59.10205	В	16.784	19.954	20.241	18.323	62.03962	в	16.850	19.713	20.002	18.304
59.10987	в	16.815	19.944	20.061	18.350	62.04743	В	16.858	19.747	20.015	18.304
59.85598	в	17.311	19.740	20.228	18.364	62.05524	B	16.843	19.728	20.057	18.304
59.86379	в	16.820	19.764	20.146	18.377	62.06306	B	16.817	19.821	20.128	18.296
59.87942	в	16.798	19.847	20.067	18.362	62.07087	B	16.800	19.838	20.246	18.458
59.88723	в	16.811	19.869	20.035	18.350	62.07868	в	16.818	19.796	20.276	18.284
						62.08649	в	16.839	19.755	20.192	18.302

TABLE 4. Photometry for H1, H2, H3, and H4.

a) Heliocentric Julian Date of mid exposure

the isochrones do fit the data reasonably well and the absolute age of M71 appears to be between 14 and 16 Gyr. H87 derive an absolute age of 13.5 ± 2 Gyr for 47 Tuc using isochrones with [Fe/H] = -0.65. To within the limits of our data we find a similar age for M71. This conclusion, which depends upon the adopted values of the reddening and distance modulus, is clearly consistent with the result of comparing the fiducials of 47 Tuc and M71. (Note that the fiducial comparison is independent of distance and reddening uncertainties and requires only that the clusters have a similar chemical composition.)

4. VARIABLE STARS IN M71

4.1 Variable Star Identification

The major purpose of this work was to search for variable stars. Although automated schemes for selecting variables from a set of data have been proposed (e.g., Shara *et al.* 1988) we found it necessary to view the light curve of each star in order to pick out the variables. This leads to the possibility of having not correctly identified some small amplitude variables. A total of four variables were discovered in the field under investigation. Photometry for these stars is given in Table 4. Each of these will be discussed in turn, following a brief description of the method used to analyze the periods.

Two of the variables discovered had sufficient phase coverage to allow the use of a Fourier analysis technique to determine their periods. The approach used followed that of Deeming (1975), as modified by Kurtz (1985), and Matthews & Wehlau (1985). This latter modification uses trigonometric identities to reduce computing time when calculating the Fourier components. The program used for this analysis was supplied by J. M. Matthews, and subtracts the mean of the dataset so as to remove any long term trends (as noted in Deeming's paper) before the analysis commences. The usual approach adopted for this work was to first conduct an initial period analysis over a fairly wide range of frequencies; here 0-100 cycles per day (c/d) with a grid of 2000 frequencies. Then a more detailed analysis using a finer frequency grid was used to narrow down onto the most prominent peaks. Although there was often sufficient phase coverage to determine a period in this way, the lack of an extended temporal baseline of observations led to aliasing

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FIG. 3. A comparison between the principle sequences of M71 (solid curve, from the current work) and 47 Tuc (dashed curve, from Hesser *et al.* 1987). The latter have been shifted by 0.379 in V and 0.235 in B - Vfollowing the procedure in VandenBerg *et al.* (1990). The dot at V = 14.44, B - V = 1.06 represents the M71 horizontal branch.

problems in the amplitude spectra, making the precise determination of a true period difficult. Furthermore it was noted that the B data was of significantly poorer quality than the Vdata and was consequently excluded from the periodogram analysis.

4.2 Variable H1

H1 (star 81 in Table 2) is in the blue straggler region of the CMD (see Fig. 1). We have identified this star with the star KC-211 from Cudworth (1985) who assigns it a cluster membership probability of only 42% based upon its proper motion. However the V magnitude of this star is close to Cudworth's limiting magnitude, and is in a fairly crowded portion of the field, so we will continue with the following discussion under the assumption that H1 is a cluster member. Figure 5(a) shows the light curve for this star for the first, second, and fourth nights of observations. Figure 5(b) shows similar data for a star (number 385 in Table 2) of similar magnitude and position as H1 for comparison purposes. Figure 5(c) shows the resultant amplitude spectrum from 0 to 50 c/d with a spacing of 0.01 c/d. The highest peak, with an amplitude of 0^m055, at approximately 19.96 c/d, corresponds to a period of 04050. There are significant aliasing problems in the data, as can be seen in this figure and other possible periods include 04055, 04053, and 04046.

However the best phase diagram is obtained for the period of 04050, shown in Fig. 5(d).

Variable H1 appears to be a variable blue straggler of the SX Phe type (Nemec 1989). This is the first such star to be found in the vicinity of a metal-rich globular cluster, al-though they are known in the metal-poor globular cluster NGC 5466 (Mateo *et al.* 1990) and in ω Cen (Jørgensen 1982; Jørgensen & Hansen 1984; DaCosta & Norris 1988). For a cluster distance modulus of 13.70 ± 0.20 (Richer & Fahlman 1988), the mean V magnitude of 16.252 ± 0.006 leads to an absolute magnitude $\langle M_V \rangle = 2.55 \pm 0.20$. If the star is placed on the period-luminosity relation shown in Fig. 7 of Nemec (1989) one sees that it is most probably a first overtone mode pulsator.

Knowing the absolute magnitude and the pulsation period, the mass of H1 can be derived from the period-mean density relation (see, for example, van Albada & Baker 1971) of which Nemec & Mateo (1991) give the variant

$$\log \frac{\mathcal{M}}{\mathcal{M}_{\odot}} = 2 \log \frac{Q_m}{P_m} - 0.6M_{\rm bol} - 6 \log T_e + 25.40, (1)$$

where the subscript *m* refers to the pulsation mode and M_{bol} is the bolometric magnitude. *P* and ρ are the period and mean density respectively. The pulsation constant *Q* was

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taken to be 0.0333 for the fundamental mode and 0.0252 for the first overtone mode (Petersen & Jørgensen 1972). Errors of 10% in these quantities were assumed. The error of the period was derived by fitting a parabola to 21 points from the amplitude spectrum—the peak point at 19.96 c/d, together with 10 points on either side. Errors in the fitting parameters led to an error of 040004 in the position of the peak. Values for the effective temperature (of 7900 \pm 400 K) and the bolometric correction (B.C.) ($-0m11 \pm 0.05$) were obtained by interpolation of Table 66 of Lang (1986). The errors in the quantities calculated from these tables are "worst case" estimates.

Assuming a first overtone pulsation mode, we derive a mass of

$$\mathcal{M}_{\rm H1} = (0.90 \pm 0.47) \mathcal{M}_{\odot}$$

22

0.6

0.8

1.0

B-V

1.2

1.4

0.6

0.8

1.0

B-V

1.2

1.4

where the error in the mass was calculated using standard error propagation techniques. Note that if the star is pulsating in the fundamental mode the following mass results:

$$\mathcal{M}_{\rm H1} = (1.58 \pm 0.83) \mathcal{M}_{\odot}.$$

The mass we derive for H1 (assuming a first overtone mode of pulsation) is somewhat lower than the mean mass of most SX Phe stars. The derived masses of all known SX Phe variables lie in the range ~1.0 to ~1.6 \mathcal{M}_{\odot} with a mean mass of ~1.2 \mathcal{M}_{\odot} (Nemec 1989; Nemec & Mateo 1990).

Nemec & Harris (1987) have also computed (via dynamical arguments) the mean mass of all the blue stragglers in NGC 5466 to be $\sim 1.2 \mathcal{M}_{\odot}$. Given the large uncertainty associated with the result, our estimate of the mass of H1 is consistent with the hypothesis that it is an SX Phe star in M71. Note that if a mass of $\sim 1.2 \mathcal{M}_{\odot}$ is adopted for H1, the required distance modulus of the star is 13.9, which is within the allowed uncertainty of the M71 distance modulus.

4.3 Variable H2

H2 (1152 in Table 2) appears on Fig. 1 to be a faint, very blue star, lying approximately 1 $^{m}75$ below the main sequence turnoff point. The light curve for H2 is shown in Fig. 6(a). Figure 6(b) shows the light curve for a comparison star to H2 (star 1215 in Table 2). The initial amplitude spectrum generated for the V data revealed several strong peaks around 17 c/d, five of which gave reasonably good phase diagrams (these were at 16.5303, 16.8503, 17.1803, 17.5103, and 17.8403 c/d). A second amplitude spectrum was obtained using a frequency grid with an interval of 0.01 c/d over a range 10–30 c/d. This is shown in Fig. 6(c) where the effect of the alias frequency of around 1 c/d can also be seen. The strongest peak, with an amplitude of 0 $^{m}053$ and a period of 0 $^{q}0582$ was found to produce the best phase diagram in that it had the least dispersion about a sine curve.

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FIG. 5. (a) The light curve for the variable H1. Data for the first, second and fourth nights of observation are plotted in the upper, middle, and lower panels, respectively. (b) A similar plot for star 385 of Table 2, of comparable magnitude, and similar position in the field. In these, and the plots of a similar nature that follow these two, the error bars returned by DAOPHOT have been plotted but are generally smaller than the symbols used to plot the points. (c) An amplitude spectrum generated using the data shown above. The maximum peak of 19.3 c/d is indicated. (d) A phased light curve generated from the data shown above with a period of 04050. The epoch for the phasing was chosen to be HJD 2446261.96540, the heliocentric Julian Date of the brightest magnitude in the sequence.

As seen in Fig. 1, H2 lies blueward of the main sequence, below the turnoff point near to the white dwarf/hot subdwarf region of the CMD (Richer & Fahlman 1988; Drukier *et al.* 1989). The photometry of Richer & Fahlman (1988) verifies the blue color of this star. If this star is indeed a cluster member then its position in the CMD is quite unusual. With such a low luminosity and a period typical of a dwarf Cepheid, it is possible that this is a field star superimposed on the cluster. On the other hand, Kaluzny (1989) has



FIG. 6. (a) The light curve for the variable H2. The plot is similar in fashion to Fig. 5(a). (b) A similar plot for star 1215 of Table 2, of comparable magnitude and similar position in the field. (c) An amplitude spectrum generated using the data shown above. (d) A phased light curve generated from the data shown above with a period of 040582 corresponding to the frequency of the central (and highest) peak in the amplitude spectrum. The phasing epoch was HJD 2446261.96930.

shown the existence of an "extension" of the blue straggler sequence down to the left of the main sequence in the cluster NGC 188. *If* the star H2 found in this study is a member of M71 and is similar to the NGC 188 stars then it may imply an extension of the instability strip down to these low luminosities. We note that the shape of the light curve suggests that it is unlikely to be a W UMa type binary.

4.4 Variable H3

In Fig. 1 the variable H3 (star 865 in Table 2) lies well to the right of the main sequence, suggesting that it may be a

field star. The light curve is shown in Fig. 7(a), with a comparison star shown in Fig. 7(b) (star 935 in Table 2). It appears to be more like that of an eclipsing binary star than that of a pulsator. From Fig. 7(a) it can be seen that there is insufficient phase coverage for any accurate periods to be determined. Despite this, an amplitude spectrum was generated from the V data in the manner described above. It showed several peaks in the region 3-8 c/d, the highest being at 5.37 c/d. In an examination of the B data, two peaks of significant amplitude were found at 5.37 and 10.40 c/d. In order to try and increase the phase coverage the two sets of data were then merged by normalizing the B data to the Vdata. The most noticeable features were peaks at 4.39 and 5.37 c/d. It was found that the latter frequency (a period of 0^d186) produced the best phase diagram, though there are substantial gaps in the phase coverage.

The shape of the light curve for this star is unusual. If it is a binary star, such as a W UMa type variable, the $0^{4}186$ period should be doubled to give $0^{4}372$. However the shape of the light curve is not a good match to other W UMa variables [e.g., the stars NH19 and NH30 in NGC 5466 (Nemec & Harris 1987; Mateo *et al.* 1990)]. Further investigation of this star is required to confirm or refute its variability.

4.5 Variable H4

No period analysis could be done on variable H4 (star 333 in Table 2) since it appears that only one cycle has been observed [see Fig. 8(a)]. Figure 8(b) shows the light curve for star 80 (Table 2), included for comparison purposes. The shape of the light curve is strongly suggestive of an eclipsing binary system. If verified this would be of some interest because (excluding W UMa stars) there is only one other eclipsing binary positively identified in a globular cluster. That star is NJL5 in ω Cen, discovered by Niss *et al.* (1978)



FIG. 7. (a) The light curve for the variable H3. The plot is similar in fashion to Fig. 5(a). (b) A similar plot for star 935 of Table 2, of comparable magnitude and similar position in the field.



FIG. 8. (a) The light curve for the variable H4. The plot is similar in fashion to Fig. 5(a). (b) A similar plot for star 80 of Table 2 of comparable magnitude and similar position in the field. This star was identified by Cudworth (1985) as KC-371.

and confirmed as being a radial velocity member of ω Cen by Jensen & Jørgensen (1985) and Margon & Cannon (1989). However in our case the star H4 seems peculiarly placed on the M71 CMD and radial velocity information would be required to confirm membership for H4.

5. SUMMARY

Using deep CCD photometry we have constructed a CMD of M71 and compared this to the theoretical isochrones of Bergbusch & VandenBerg (1991). Within the accuracy of our data we find no significant age difference between M71 and 47 Tuc when using the method proposed by VandenBerg *et al.* (1991). We note that this determination is critically dependent on the definition of the fiducial sequence near the main sequence turnoff and extending up the lower red giant branch. This fiducial is not well defined by our photometry. Hence the possibility of a relative age difference between 47 Tuc and M71 remains open. The absolute age of M71 obtained by overlaying the isochrones on the CMD appears to be between 14 and 16 Gyr.

A total of 989 stars in a field of M71 were examined for variability on 75 CCD frames. Of these, only four seem to be variable. Variable seeing, and the lack of sufficiently extensive phase coverage, has certainly affected the ability to detect low amplitude variability. One of the ~ 10 blue stragglers in the variable search field was found to be variable (H1). Its period and luminosity are consistent with it being an SX Phe type variable, similar to those found in other globular clusters. A second variable (H2) may very well be a field dwarf Cepheid.

Two possible binary stars were also found. The first of these (H3) has a period consistent with it being a W UMa star. These have also been found in the blue straggler region of other clusters—however this star lies to the red side of the

main sequence and may also be a field star. The second possible binary lies close to the blue straggler region. Further work is required to confirm the variability of this star.

No main sequence binaries were found in the variable search field, and from the CMD of the larger field there is no evidence of a "binary sequence" $\sim 0^{m}75$ above the main sequence. However it is likely that we do not have a large enough sample to properly address that question. By simply summing the magnitudes of the stars with $V \leq 23$ listed in Table 2, we calculate that the total integrated light in the larger survey is $9^{m}03$. On the same basis the integrated magnitude of the variable search field is $10^{m}35$. Harris & Racine (1979) give the integrated absolute magnitude of the cluster as $-5^{m}6$, which together with a distance modulus of 13.70 (Richer & Fahlman 1988) implies that we have sampled 42% and 13% of the cluster light, respectively. Thus there may be, very approximately, ~ 25 more variables in M71, of which ~ 7 may be SX Phe stars.

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